# Performance Evaluation of Elevated Storage Reservoir with Hybrid Staging 

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#### Abstract

Elevated water tanks are essential Civil Engineering framework which are known as compulsory community services urban areas. A number of elevated water tanks suffered collapse and damage to their staging in deep earthquakes, consequently their safety performance is a crucial concern throughout effective earthquake. Because of storage of clean water, it is utilized for important needs such as drinking purpose and for other domestic purpose. Within the existing work, four support patterns viz. easy brace, cross brace, rectangular brace as well as radial brace connected with various staging heights (fifteen m , twenty m , and twenty-five m ) are analysed for seismic zone II, III and IV for empty tank and loaded tank. Probably the most affordable as well as secure, Intze style tank of thousand kilolitre capacity considered. When it comes to the evaluation of Intze container, 72 designs are constructed with STAAD.ProV8i Software, by which 36 models are analysed for empty tank and additional 36 models are analysed for loaded tank. Each and every seismic zone has 12 models as well as every brace has three distinct staging rises. For the safety, stability and serviceability, different parameters are obtained for different brace pattern.


Key words : Intze container, Earthquake effect, Tank staging with brackets, STAAD.Pro. V8i.

## 1. INTRODUCTION

### 1.1 General

Water is an essential commodity for all living as well as non-living beings. Elevated water tanks are an overhead framework built with an adequate level to pressurize a normal water source process for division of water and it is utilized the place that the ground storage tanks can't be constructed because of not enough adequate natural elevation. Elevated water tanks are among the most crucial public utility constructions because they form an important aspect of the water distribution process.


Fig 1.1 Failure of braces because of earthquake
Beams and column of staging of water tanks provides the conception connection with frame structure of water tank. The mechanism of beams and column is extremely different with water tank staging model because of the large load of the container. As the failures of water tanks are always occurs within the staging system of elevated water tanks, it becomes necessary to develop an energetic fascination with checking out the powerful behaviour on the staging system.

### 1.2 Shape of Elevated Water Tank

The shape of the water tank plays a crucial economic role within the overall structure. The form of elevated water tank is frequently governed by the capacity of container. Capacity of container is the volume of water stores in water tank as per its design and style.

### 1.3 Dynamic Behaviour of Elevated Water Tank <br> The elevated water tank is top heavy structures and the structure can be assumed as an individual

degree freedom program. The weight of staging (braces and column) might be sits in the C.G. on the tank, and also the whole load on the pot is transferred towards the floor on the tank and that plays a role in every column. The container is a huge rigid framework which is very tall and there is simply no distant relative motion involve in the components on the tank and also top of the frame. Thus, absolutely no dynamic forces are caused within the container because of the variation on the frame.

### 1.4 Layout of Elevated Water Tank

The affordable size and shape of an elevated water tank are depended on a few purposeful needs like as:
a) Tank capacity
b) The optimum level for water
c) Staging heights
d) Number of braces as well as their frame type
e) Allowable bearing capability of foundation
f) Seismic zone as well as Site conditions

### 1.5 Problem Statement

Elevated water tanks are visible from near as well as from long distances. They often become landmarks on the landscape due to their shape, form and support system. Therefore, it becomes important to receive attention from the point of aesthetics. Innovations in the shape and form should be encouraged when they improve the ambience and enhance the quality of the environment.

### 1.6 Scope of project

- To analyse an Intze water tank with different horizontal braces in staging using response spectrum analysis with the help of STAAD.ProV8i.
- To study the behaviour of Intze tank on the different rise of staging in seismic zones II, III and IV.
- Comparative study of various parameters of tank with different braced system at empty and filled condition in different seismic zones.
- To obtain most efficient, stable and durable horizontal brace system for Intze tank.


### 1.7 Objective

i. To develop models of ESR with conventional and hybrid staging systems.
ii. To check performance of ESR under seismic forces by using software.
iii. To suggest suitable hybrid staging system for ESR.
iv. To study the different shapes of ESR

### 1.8 Types of Staging System Used

In the present study four types of arrangements have been considered i.e normal, cross, radial and rectangular as shown in Figure


Fig. 1.2: Different types of staging arrangements

## 2. LITERATURE REVIEW

### 2.1 General

Elevated water tanks are an essential component of water supply layout within huge cities as well as within the countryside region. Of history years, a selection of elevated water tanks has collapsed in various places across the world because of the diverse dynamics of loadings. Failure of water tanks is definitely a huge loss of property and life. The seismic analysis is important but a lot of complex for strengthening the elevated tanks. This particular chapter deals having a short overview of recent and past research of seismic result on the balance of elevated water tanks.

### 2.2 Review of the Previous Study

Significant research information of elevated water tank is summarizing inside paragraphs. Each paper is discussed with the effective results of it's as well as things that impact the overall performance of elevated water tanks
A. H. Shrigondekar et.al (2017) (1) has studied and analysed the reinforced concrete elevated tank with linear dynamic method and seismic response such as base shear, tank displacement having different types of staging configuration by using finite element method software. Sonali M. Pole et. al (2017) (2) This paper presents seismic analysis of elevated water tank with different storage capacities having different staging patterns. They compared two different supporting systems like radial bracing and cross bracing with basic
supporting system by considering various fluid level condition. By using STAAD Pro V8i software base shear, overturning moment ant displacement have been observed and then compared. Keyur Y. Prajapati et al. (2014) (3) This paper presents the analysis of hybrid staging of ESR by considering seismic loading and analysed with SAP 2000. It compared the frame type and shaft type staging systems of ESR. The main aim of this paper is to compare the cost of hybrid staging system of ESR. Mr. Santosh Rathod et. al (2018) (4) In this paper, reinforced cement concrete overhead water tank of capacity one lakh litre is considered for the analysis. Comparison is done with different staging height and base width. Analysis is carried out by STAAD Pro software. Tank level, seismic zone III considered for comparative study of bending moment, shear force and displacement. Kaviti Harsha et.al (2015) (5) has designed the Intze water tank as per IS: 3370-2009 and draft code1893-part 2, considering two mass modal method. Analysis is carried out by STAAD Pro for wind and seismic forces. Sneha Adhikari et al. (2016) (6) has compared the Intze tank with inclined bracing (single inclined bracing and cross inclined bracing) with alternate layers at staging and inclined bracing throughout height of staging. Overall analysis is carried out as per draft code of IS 1893 (part 2) by using STAAD Pro software. P. S. Nemade et al. (2016) (7) has analysed different bracing patterns in staging configuration of ESR by using STAAD Pro software. Analysis carried out by considering different seismic zones 3,4 and 5 and also consider empty and full condition of tank for analysis. Manish N. Gandhi. et.al (2016) (8) has study the behaviour of different staging patterns of circular elevated tank for better performance during earthquake. It includes the different bracing types for the analysis using STAAD Pro software. Base shear and maximum displacement in $\mathrm{X}, \mathrm{Y}$ and Z direction of circular tank is compared. Prashant A. Bansode et al. (2017) (9) has review the Seismic Analysis of Elevated Water Tank with as well as while not bracing with frame staging. The various forms of bracing are cross bracing as well as diagonal bracing with zone III by reaction spectrum strategy as per Is actually 1893 (Part II) 2014 as well as Seismic a lot are given as per Is actually: 1893:2002 (Part II) applying STAAD Pro V8i 2007 application. Ayazhussain M. Jabar et. al (2012) (10) In this paper two different systems are taken into consideration for the proposed work. Results from staging with basic pattern, staging with radial bracing and staging with cross bracing at various fluid level condition are compared here. To understand the seismic behaviour on elevated
water tank they compared base shear, overturning moment, roof displacement at different staging type and different filled conditions of water tank.

## 3. RESEARCH METHODOLOGY

### 3.1 General

This particular project work includes the "Seismic Analysis of Intze Water Tank with different Bracing Configurations." To handle the analysis, different IS codes are used to evaluation of elevated water tank.

### 3.2 Categories of Loads

### 3.2.1 Dead Load

The fixed load for any structure is known as dead load. For overhead water tank, fixed elements like column, bracing, bottom ring beam, top ring beam, cylindrical walls, top dome, bottom dome weight that required on ground.

### 3.2.2 Imposed Load

When a load due to temporary objects and load other than dead load is known as imposed load. This particular load arises through the planned utilization of occupancy or structure of all of the structure. Various types of imposed loads coming on structure are given in IS: 875 (Part 2) - 1987. For overhead water tank, hydrostatic stress within cylindrical walls and bottom dome is a result of development of waves in the course of seismic outcome.

### 3.2.3 Wind Load

In almost any framework, load by the speed of wind and the density of it is known as wind load. In order to fight the result of breeze load, constructions are intended accordance IS: 875 (part 3) - 1987. Wind load is depend upon the velocity of wind and also design of any structure.

### 3.2.4 Seismic Forces

Seismic forces are one of the primary parts of force each time a system is examined as well as created. As seismic outcome leads to shacking of the ground, therefore the framework on the ground should be stable from its base.

### 3.2.5 Load Combination

Different load mixture of elevated water tanks is offered to protect the crucial condition during design and analysis. Is 1893 (part one): 2016 is utilized for load combinations, this particular code deals with effects of loads. In addition, it likewise consists of load combination guidelines. The next load combinations with a suitable factor of safety might be pushed based on Indian standard format.

$$
\begin{aligned}
& \bullet 1.2(\mathrm{DL}+\mathrm{IL}+\mathrm{EL}) \\
& \bullet 1.2(\mathrm{DL}+\mathrm{IL}-\mathrm{EL}) \\
& \bullet 1.5(\mathrm{DL}+\mathrm{EL}) \\
& \bullet 1.5(\mathrm{DL}-\mathrm{EL})
\end{aligned}
$$

- 0.9 DL + 1.5 EL
- 0.9 DL-1.5 EL

Where,
DL = Dead Load
LL=Live Load
EL= Earthquake Load

### 3.3 Part of Intze Tank

A container is utilized to storage of water for a lot of uses (drinking clean water, sprinkler system farming, fire suppression etc.). Based on different code provisions we have been performed different element designs

### 3.4 Materials used for Elevated Water Tanks

In order to make a leak-proof container, well graded mix having low porosity and high tensile strength is suitable. As per IS: 3370 , the minimum grade of concrete required for construction of water tank is M20 for plain concrete, M30 for reinforced cement concrete and M40 for prestressed cement concrete and as per IS: 1786-2008 Fe 415 have been used as reinforcement for water tanks.

### 3.5 Seismic Analysis Method

In India, almost all RCC structure components in various zones are seismically examined for a regular earthquake. It provides the estimation of reaction produced by the framework due to earthquake. System subjected to earthquake is examined by various approaches to seismic evaluation.
I. Response Spectrum Analysis.
II. Time History Analysis.

### 3.5.1 Factor Influencing Response Spectrum

- Energy releases mechanism.
- Soil condition of zone and type of soil.
- Damping in the structure system.
- Time period of the system.


### 3.6 Computation of Dynamic Quantity

The code IS: 1893 (Part 2) is used for evaluation of the heightened water tanks.

### 3.6.1 Horizontal Seismic Coefficient

The seismic coefficient Ah will probably be estimated by utilizing formula

$$
A_{h}=\frac{Z}{2} \times \frac{S_{a}}{g} \times \frac{I}{R}
$$

Where,

$$
\mathrm{Z}=\mathrm{Zone} \text { factor as per Table } 2 \text { of IS }
$$

1893 (Part 1)-2002

I = Importance factor as per Table 1 of IS 1893 (Part 2)-2002,
$\mathrm{R}=$ Response reduction factor as per Table 2 of IS 1893 (Part 2)-2002,
$\mathrm{Sa} / \mathrm{g}=$ Average response acceleration coefficient as given by Fig. 2 and
table 3 of IS 1893 (Part 1)-2002 and subjected to clause 4.5 .1 to 4.5 .4 of standard.

### 3.6.2 Base Shear

The base shear for elevated tank on impulsive mode, just about the base of staging is given by $\mathrm{Vi}=(\mathrm{Ah}) \mathrm{i}(\mathrm{mi}+\mathrm{ms}) \mathrm{g}$ Where,
$(A h) i=$ horizontal seismic coefficient for impulsive mode,
$\mathrm{mi}=$ impulsive mass of liquid on container,
$\mathrm{ms}=$ mass of container one-third mass of staging,
$\mathrm{g}=$ acceleration due to gravity.
And in convective mode the base shear is given by

$$
V_{c}=\left(A_{h}\right)_{c} m_{c} g
$$

$(\mathrm{Ah}) \mathrm{c}=$ horizontal seismic coefficient for convective mode,
$\mathrm{mc}=$ convective mass of liquid on container.
So the base shear will be obtained by combining the impulsive and convective mode base shear and is given as

$$
\mathrm{V}=\sqrt{ } \mathrm{V}_{\mathrm{i}}^{2}+\mathrm{V}_{\mathrm{c}}{ }^{2}
$$

Where
$\mathrm{V}=$ total base shear by elevated tank,
$\mathrm{Vi}=$ base shear in impulsive mode,
$\mathrm{Vc}=$ base shear in convective mode.

### 3.6.3 Base Moment

As per IS 1893 (part 2) -2002 clause 4.7, Overturning moment at the base of staging for impulsive mode

$$
\mathrm{M}_{\mathrm{i}}=\left(\mathrm{A}_{\mathrm{h}}\right)_{\mathrm{i}}\left[\mathrm{~m}_{\mathrm{i}}\left(\mathrm{~h}_{\mathrm{i}}+\mathrm{h}_{\mathrm{s}}\right)+\mathrm{m}_{\mathrm{s}} \mathrm{~h}_{\mathrm{cg}}\right] \mathrm{g}
$$

And on convective mode is given by
$\mathrm{M}_{\mathrm{c}}=\left(\mathrm{A}_{\mathrm{h}}\right)_{\mathrm{c}} \mathrm{m}_{\mathrm{c}}\left(\mathrm{h}_{\mathrm{c}}+\mathrm{h}_{\mathrm{s}}\right) \mathrm{g}$
Where,
$\mathrm{hs}=$ structural height of staging,
measured from top of footing of staging
to the bottom of tank wall
hcg $=$ height of center of gravity of
empty container, measured from base of
staging

Total base moment shell be obtained by square of sum of squares in both impulsive and convective modes given as follow

$$
\mathrm{M}=\sqrt{ } \mathrm{M}_{\mathrm{i}}^{2}+\mathrm{M}_{\mathrm{c}}^{2}
$$

Where,
$\mathrm{M}=$ total overturning moment or base moment,
$\mathrm{Mi}=$ base moment in impulsive mode of tank at base,
$\mathrm{Mc}=$ base moment in convective mode of tank at base.

### 3.6.4 Time Period

As per IS 1893 (part 2) -2002, clause 4.3,
The period of impulsive mode of an elevated tank
$\mathrm{T}_{\mathrm{i}}=2 \pi \sqrt{ }\left(\mathrm{~m}_{\mathrm{i}}+\mathrm{m}_{\mathrm{s}} / \mathrm{K}_{\mathrm{s}}\right)$
Where,
$\mathrm{mi}=$ impulsive mass of liquid on container
$\mathrm{ms}=$ mass of container one-third mass of staging
$\mathrm{Ks}=$ lateral stiffness of staging
The period of convective mode
$\mathrm{T}_{\mathrm{c}}=2 \pi \sqrt{ }\left(\mathrm{~m}_{\mathrm{c}} / \mathrm{K}_{\mathrm{c}}\right)$
$\mathrm{mc}=$ convective mass of liquid on container
$\mathrm{Kc}=$ stiffness of convective mode

### 3.6.5 Hydrodynamic Pressure

The pressure exerted by the liquid in the tank as per IS 1893 (part 2)-2002 clause 4.9,

$$
\mathrm{P}=\mathrm{Q}(\mathrm{y})\left(\mathrm{A}_{\mathrm{h}}\right)_{\mathrm{i}} \rho \mathrm{gh} \cos \phi
$$

$\mathrm{Q}(\mathrm{y})=0.866[1-(\mathrm{y} / \mathrm{h}) 2] \tanh [0.866(\mathrm{D} / \mathrm{h})]$ Where
$\mathrm{P}=$ hydrodynamic pressure on tank wall,
$\mathrm{Q}=$ of pressure on tank wall,
$\rho=$ mass density of liquid,
$\phi=$ circumferential angle,
$h=$ maximum depth of liquid,
$y=$ vertical distance of a point on tank wall from bottom of tank wall.

### 3.6.6 Pressure due to Wall Inertia

As per IS 1893 (part 2)-2002 clause 4.9.5, Pressure on the tank wall due to its inertia is given by

$$
\mathrm{P}_{\mathrm{ww}}=\left(\mathrm{A}_{\mathrm{h}}\right)_{\mathrm{i}} \mathrm{t} \rho_{\mathrm{m}} \mathrm{~g}
$$

Where,
$\rho_{\mathrm{m}}=$ mass density of tank wall,
$\mathrm{t}=$ thickness of wall.
Table 3.1 Intze tank version detail

| Sr. No. | Name of <br> parameter | Value of parameter |
| :---: | :--- | :--- |
| 1. | Seismic zones | II, III, IV |
| 2. | Seismic zone factor | 1. II $=0.10$ <br> 2. III $=0.16$ <br> 3. IV $=0.24$ |
| 3. | Types of bracing <br> pattern | 1. Simple bracing. <br> 2. Cross bracing. <br> 3. Radial bracing. <br> 4. Rectangular bracing. |


| 4. | Condition | 1. Tank Full <br> 2. Tank Empty |
| :---: | :---: | :---: |
| 5. | Height of staging | $15 \mathrm{~m}, 20 \mathrm{~m}, 25 \mathrm{~m}$ |
| 6. | Number of column | 8 |
| 7. | Soil type | Medium soil |
| 8. | Types of support | Fixed support |
| 9. | Response reduction factor | 2.5 |
| 10. | Importance factor <br> (I) | 1.5 |
| 11. | Damping ratio | $5 \%$ |
| 12. | $\begin{aligned} & \text { Capacity of } \operatorname{tank}(\mathrm{V}) \\ & \text { in } k L \end{aligned}$ | 1000 |
| 13. | Diameter of cylindrical wall | 15.57 m |
| 14. | Rise of top dome | 3.081 m |
| 15. | Thickness of top dome | 0.08 m |
| 16. | Top ring beam | $0.2 \times 0.2 \mathrm{~m} 2$ |
| 17. | Thickness of cylindrical wall | 0.17 m |
| 18. | Height of cylindrical wall | 4.622 m |
| 19. | Middle ring beam length | 1 m |
| 20. | Middle ring beam height | 0.25 m |
| 21. | Height of conical wall | 2.309 m |
| 22. | Thickness of conical wall | 0.38 m |
| 23. | Diameter of bottom dome | 11.40 m |
| 24. | Rise of bottom dome | 2.156 |
| 25. | Thickness of bottom dome | 0.38 m |
| 26. | Bottom ring beam | $1.25 \times 0.62 \mathrm{~m} 2$ |
| 27. | Brace size | $0.6 \times 0.4 \mathrm{~m} 2$ |
| 28. | Number of braces on tank | 4 |
| 29. | Number of column on tank | 8 |
| 30. | Angle of inclination of conical dome | 450 |
| 31. | Semi central angle of bottom dome | 440 |

### 3.7. Bracing Pattern on Intze Tank

Water tank without brace cannot avoid bent, rotations and twisting around its vertical axis. Therefore, the framework requires braces for supporting them in all of the circumstance. As stated by IS: 11682 - 1985, when the level of staging is more than 6 m previously cosmetic foundation, the column shall require of horizontal bracing. Within this study we're planning to make use of 4 kinds of brace with staging process. Figures indicates 2
dimensional and 3 dimensional models of braces in STAAD.ProV8i. as uses.


Fig. 3.1 2D and 3D simple type brace staging model


Fig 3.2 2D and 3D cross type brace staging model


Fig 3.3-2D and 3D radial type brace staging model


Fig 3.4 2D and 3D rectangular type brace

## staging model

## 4. RESULT AND DISCUSSION

### 4.1 General

The evaluation contains variables for simple, rectangular, radial and cross style braces connected with three distinct staging heights i.e. $15 \mathrm{~m}, 20 \mathrm{~m}$ as well as 25 m within seismic zones II, III and IV. Various tables \& charts are indicating the different details as displacement, shear force, axial force, torsion, bending moment.

### 4.2 Results and Discussion

### 4.2.1 Displacement

Displacement within elevated water tanks indicates the movement of tank from its original position to the next position within the horizontal path. The specified final results present the maximum displacement values get as a result of the evaluation on the water tank which may occur at condition that is extreme. Outcomes are examined about the bases of most tank problems i.e. empty as well as loaded, with various kinds of braces in staging for several heights that evaluation for seismic zones II, III and IV.

Table 4.1 Displacement values during the empty state of tank in seismic zones II, III and IV

| Braces on <br> tank | Height of <br> staging <br> $(\mathbf{m})$ | Maximum Displacement (mm) |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Zone II | Zone III | Zone IV |  |
| Simple <br> brace | 15 m | 14.807 | 23.391 | 34.922 |
|  | 20 m | 26.287 | 41.787 | 62.530 |
|  | 25 m | 41.483 | 66.116 | 99.031 |
| Rectangular <br> brace | 15 m | 13.891 | 21.879 | 32.625 |
|  | 20 m | 24.744 | 39.750 | 58.550 |
|  | 25 m | 38.595 | 61.449 | 92.007 |
|  | 15 m | 14.029 | 22.094 | 32.944 |
|  | 25 m | 24.595 | 39.022 | 58.354 |
| Radial brace | 20 m | 24.592 | 39.015 | 58.341 |
|  | 25 m | 38.327 | 61.007 | 91.336 |



Fig. 4.1 Displacement graph for various kinds of braces in staging during the empty situation of tank in seismic zone II


Fig. 4.2 Displacement graph for various kinds of braces in staging during the empty state of tank in seismic zone III


Fig. 4.3 Displacement graph for various kind of braces in staging during the empty situation of tank in seismic zone IV

Table 4.1 shows the horizontal displacement by tank staging on the time of empty state of tank. Fig. 4.1, 4.2 and 4.3 are plotted for displacement (mm) versus types of braces in staging for $15 \mathrm{~m}, 20 \mathrm{~m}$, and 25 m staging height in seismic zone II, III and IV respectively. Within seismic zones II, III and IV, the maximum horizontal displacement for 15 m staging height is shown by simple type brace staging and decreases for radial type brace staging and cross type brace staging and the minimum displacement is shown by rectangular type brace staging. For 20 m as well as 25 m staging heights, the optimum displacement is shown by simple type brace staging and it decreases for rectangular type brace staging as well as for cross type brace and minimum value of displacement is shown by radial brace staging within just about all seismic zones.

Table 4.2 Displacement values in the loaded condition of tank in seismic zones II, III and IV

| Braces on <br> tank | Height of <br> staging (m) | Maximum Displacement (mm) |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Zon <br> e II | Zon <br> e III | Zo <br> ne <br> IV |  |
|  | 15 m | 20.1 | 29.4 | 42. |

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|  | 20m | $\begin{gathered} 33.4 \\ 04 \end{gathered}$ | $\begin{gathered} \hline 50.7 \\ 26 \end{gathered}$ | $\begin{aligned} & 74 . \\ & 674 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: |
|  | 25m | $\begin{gathered} 50.8 \\ 60 \end{gathered}$ | $\begin{gathered} 78.8 \\ 65 \end{gathered}$ | $\begin{gathered} 116 \\ .97 \\ 1 \end{gathered}$ |
| Rectangul ar brace | 15m | $\begin{gathered} 19.0 \\ 59 \end{gathered}$ | $\begin{gathered} 27.5 \\ 20 \end{gathered}$ | $\begin{aligned} & 39 . \\ & 423 \end{aligned}$ |
|  | 20m | $\begin{gathered} 31.2 \\ 37 \\ \hline \end{gathered}$ | $\begin{gathered} 47.0 \\ 02 \end{gathered}$ | $\begin{gathered} 68 . \\ 919 \end{gathered}$ |
|  | 25m | $\begin{gathered} 47.2 \\ 08 \end{gathered}$ | $\begin{gathered} 72.7 \\ 39 \end{gathered}$ | $\begin{gathered} 107 \\ .62 \\ 8 \\ \hline \end{gathered}$ |
| Cross <br> brace | 15m | $\begin{gathered} 19.1 \\ 64 \\ \hline \end{gathered}$ | $\begin{gathered} 27.6 \\ 79 \end{gathered}$ | $\begin{aligned} & 39 . \\ & 658 \end{aligned}$ |
|  | 20m | $\begin{gathered} 31.2 \\ 19 \\ \hline \end{gathered}$ | $\begin{gathered} 46.9 \\ 47 \\ \hline \end{gathered}$ | $\begin{aligned} & 68 . \\ & 821 \end{aligned}$ |
|  | 25m | $\begin{gathered} 46.8 \\ 89 \end{gathered}$ | $\begin{gathered} 72.1 \\ 87 \end{gathered}$ | $\begin{gathered} \hline 106 \\ .77 \\ 4 \\ \hline \end{gathered}$ |
| Radial brace | 15m | $\begin{gathered} \hline 19.1 \\ 86 \\ \hline \end{gathered}$ | $\begin{gathered} 27.7 \\ 08 \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 39 . \\ & 669 \\ & \hline \end{aligned}$ |
|  | 20m | $\begin{gathered} 31.1 \\ 92 \end{gathered}$ | $\begin{gathered} 46.8 \\ 93 \end{gathered}$ | $\begin{gathered} \hline 68 . \\ 733 \\ \hline \end{gathered}$ |
|  | 25m | $\begin{gathered} 46.7 \\ 58 \end{gathered}$ | $\begin{gathered} 71.9 \\ 60 \end{gathered}$ | $\begin{gathered} 106 \\ .42 \\ 3 \\ \hline \end{gathered}$ |



Fig. 4.4 Displacement graph for various kind of braces in staging in the loaded condition of tank in seismic zone II

Fig. 4.5 Displacement graph for various kind of braces in staging in the loaded condition of tank in seismic zone III


Fig. 4.6 Displacement graph for various kind of braces in staging in the loaded condition of tank in seismic zone IV

Table 4.2 shows the horizontal displacement by tank staging in the filled condition of tank. Fig. 4.4, 4.5 as well as 4.6 are plotted for displacement ( mm ) versus types of braces in staging for $15 \mathrm{~m}, 20 \mathrm{~m}$, and 25 m staging height in seismic zone II, III and IV respectively. The maximum horizontal displacement for 15 m staging level is shown by the simple type brace staging and decreases for radial type brace staging and cross type brace staging and the minimum displacement is shown by rectangular type brace staging. For 20 m as well as 25 m staging heights,
the maximum displacement is shown by simple type brace staging and decreases for rectangular type brace staging and cross type brace and the minimum value of displacement is shown by radial type brace staging within seismic zones II, III and IV.

### 4.2.2 Axial Forces

The final results show the optimum importance of axial force for various kinds of braces in staging for seismic zones II, III and IV.

Table 4.3 Axial force during the empty state of tank in seismic zones II, III and IV

| Braces on <br> tank | Height of <br> staging <br> (m) | Axial force (kN) |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Zone II | Zone III | Zone IV |  |
| Simple <br> brace | 15 m | 1288.766 | 1459.889 | 1688.054 |
|  | 20 m | 1371.095 | 1567.632 | 1829.683 |
|  | 25 m | 1447.735 | 1666.273 | 1957.660 |
| Rectangular <br> brace | 15 m | 1468.825 | 1666.121 | 1929.184 |
|  | 20 m | 1552.026 | 1777.033 | 2077.043 |
|  | 25 m | 1627.990 | 1875.980 | 2206.634 |
|  | 15 m | 1441.496 | 1628.638 | 1878.160 |
| Radial | 25 m | 1526.158 | 1740.113 | 2025.387 |
| brace | 15 m | 1453.845 | 1840.429 | 2155.875 |
|  | 20 m | 1538.427 | 1753.357 | 1893.546 |



Fig.4.7. Axial force graph for various brace staging during the empty state of tank in seismic zones II,III and IV

Table 4.3 shows the axial force for various forms of brace staging for empty tank in seismic zones II, III and IV. Fig.4.7 are plotted for axial forces for simple, cross, radial and rectangular type support staging when connected with $15 \mathrm{~m}, 20 \mathrm{~m}$ as well as 25 m staging rise. The least axial force shown by simple type support staging in seismic
zones II, III and IV and the maximum axial force values is shown by rectangular type brace staging for those zones.
Table 4.4 Axial pressure worth in the loaded
condition of tank in seismic zones II, III and IV

| Braces on <br> tank | Height <br> of <br> staging <br> (m) | Axial force (kN) |  |  |  | ZoneII | Zone III | ZoneIV |
| :---: | :---: | :--- | :--- | :--- | :---: | :---: | :---: | :---: |
|  | 15 m | 20 m | 3634.1 <br> 00 | 3837.130 |  |  |  |  |
|  | 25 m | 3802.0 <br> 55 | 3953.875 | 4262.969 |  |  |  |  |
| Rectangula <br> r brace | 20 m | 4059.312 | 4401.138 |  |  |  |  |  |
|  | 15 m | 3817.1 <br> 24 | 3906.0 <br> 69 | 4048.079 |  |  |  |  |



Fig. 4.8 Axial force graph for various support staging in the filled condition of tank in seismic zones II, III and IV

Table 4.4 shows the axial force for various forms of brace staging with the loaded tank in seismic zones II, III as well as IV. Fig. 4.8 plotted for axial force during loaded condition of tank for simple, cross, radial and rectangular type brace staging when connected with $15 \mathrm{~m}, 20 \mathrm{~m}$ as well as 25 m staging rise. The least axial force shown by the simple type brace staging in seismic zones II, III and IV and the maximum axial force values are shown by rectangular type brace staging within seismic zones.

## 5. CONCLUSION

From the software analysis data for elevated water tank with different bracing types at different staging heights following conclusions are drawn:

1. As the level of staging increases, the variables viz. displacement, shear force, axial force, torsion as well as bending moment are increases for empty as well as loaded condition of the tank.
2. From table no. 4.1 and 4.2, maximum displacement is displayed by simple type brace staging and the least displacement is shown by radial type brace staging for staging heights $15 \mathrm{~m}, 20 \mathrm{~m}$ and 25 m within seismic zones II, III and IV as shown in fig. 4.1,4.2 and 4.3 for empty tank and fig. 4.4,4.5 and 4.6 for loaded tank.
3. From table no. 4.3 and 4.4, axial force has least values at simple type brace staging and maximum for rectangular type brace staging for both empty and loaded tank in seismic zones II, III and IV as shown in fig. 4.7 and 4.8.
4. Tank with empty condition has less values for variables displacement, shear force, axial force, torsion as well as bending moment as compared to tank with loaded condition.
5. From the analysis of all structural models, rectangular type brace staging shows maximum value for torsion, shear force as well as bending moment and that is not risk-free within seismic zones II, III and IV.
6. Seismic analysis with radial type brace staging provide good balance as compared to other brace staging. Consequently, it is able to reduce the risks of collapse on the water container within seismic zones II, III and IV.

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