

A Novel Approach of Designing Insubstantial AVA operating in UWB for GPR Applications

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ABSTRACT

Ground Penetrating Radar (GPR) is one of the capable technologies for exposure and recognition of both metallic and non metallic objects masked under the ground. Bandwidth is one of the parameter for GPR system performance, very high frequencies are required for better resolution of microscopic objects. Ultra wide band GPR system can able to meet the current requirement with more efficiency. An Anti-podal Vivaldi Antenna (AVA) is proposed such that its operating frequency range varies from wideband to ultra wide band. A novel approach of designing Anti-podal Vivaldi Antenna is designed to increase the performance characteristics like gain, frequency of operation, radiation pattern, to reduce return loss, to reduce side lobes levels and to reduce the fabrication cost. In order to reduce the cost of fabrication, the substrate material preferred as denim material. The reason for choosing denim material is, it can be easily incorporated and it is homogeneous in nature. Anti-podal Vivaldi Antenna is designed, simulated using HFSS software and it is fabricated. The results obtained in the simulation process and the fabricated antennas are very relative to each other. The performance characteristics measured by simulation process achieves a maximum gain of more than 7dB and practical antenna achieves around 6.92dB with an operating frequency range from wide band to ultra wide band range from 5.2GHz to 13GHz.

Key words: Anti-podal Vivaldi Antenna, Ground penetrating Radar, Ultra wide band.

1. INTRODUCTION

Ultra wide band technology is on more demand now a day due to its attractive features. The applications of UWB include GPR, military, microwave imaging, radars etc due to its huge capacity, powerful penetration and accuracy [20]-[22], [34]-[36]. In GPR system antenna frequency is one of the prominent factors which decide the performance of the system. GPR system comprises 3 components radar gram, antenna and power supply. The control unit or radar gram emits electromagnetic radiation in to the surface of investigation, the reflected signal is collected by the antenna and display results on screen which helps GPR operator to

determine results accurately. As per the literature survey [27]-[33] higher the frequency of operation of antenna simplistic will be the penetration and better will be detection of minute particles. So considering all the design considerations a novel approach of Antipodal Vivaldi antenna which is also called as tapered slot antenna is proposed, which is co-planar broadband antenna, can be made from a solid piece of sheet metal. The name Antipodal refers to the geometry of the antennas. It refers to the antenna structure and also additional slots that are diametrically opposite to each other, one in top side (Patch) and another in bottom side (Ground). The main advantage of Vivaldi antennas are they are suitable from wide band to ultra wide band range of applications [18],[23],[25]. Theoretically also it was proved that it achieves infinite bandwidth. AVA can be widely used in many applications like radar, 5G communication devices, to identify voids in the concrete beam (civil), micrometer and millimeter-wave applications [1],[2],[24][26]. With the growing demand of small, light weight and compact antennas with high end performances, the designing of antennas is the most challenging aspect [3],[8],[11]. Referring to the exploitation of the Exponentially Tapered Slot Antenna, Antipodal Vivaldi antenna (AVA) proposed by Gazi, which used the alteration of micro strip line to balanced double sided slot line and spread out impedance bandwidth. However, its gain within the functional band was truncated and the maximum gain was not more than 8 to 9 dBi [4],[5],[9],[10].

2. ANTENNA DESIGN-1

Initially AVA is designed considering microstrip patch of proper dimensions, which depends on required frequency of operation of antenna along with the microstrip transmission line launched on denim jeans as substrate whose relative permittivity ϵ is 1.7 and $\tan \delta$ of 0.025, respectively as shown in figure 3(a) [12]-[19]. A balun structure is introduced to match 50 Ω microstrip feed line and patch antenna as the AVA is of balanced structure. The balun structure is the parallel plate transmission line which is connected into patch and microstrip feed line by slotting and uniting them [6], [7]. Generally the balun structure is developed based on the band width required, operating frequency and physical architecture. The following figure shows antenna design-1.

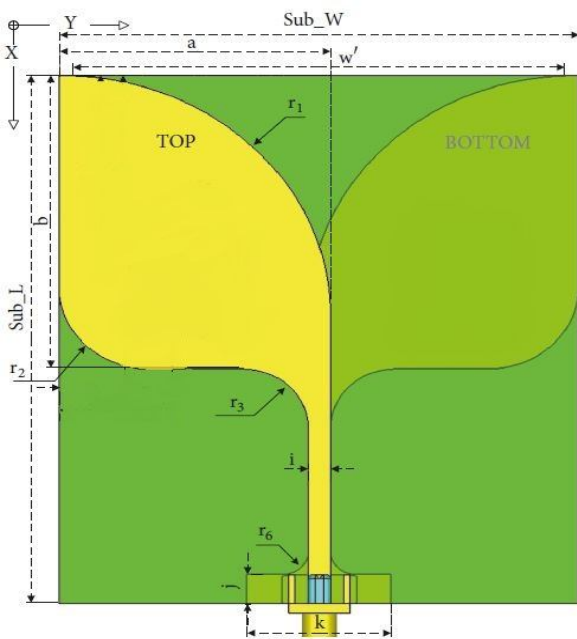


Figure 1: Designed structure of AVA without slots

2.1 Antenna Design-2

The novelty in the design of antenna is shown in figure 2 by creating a flower shape slots on patch and ground.

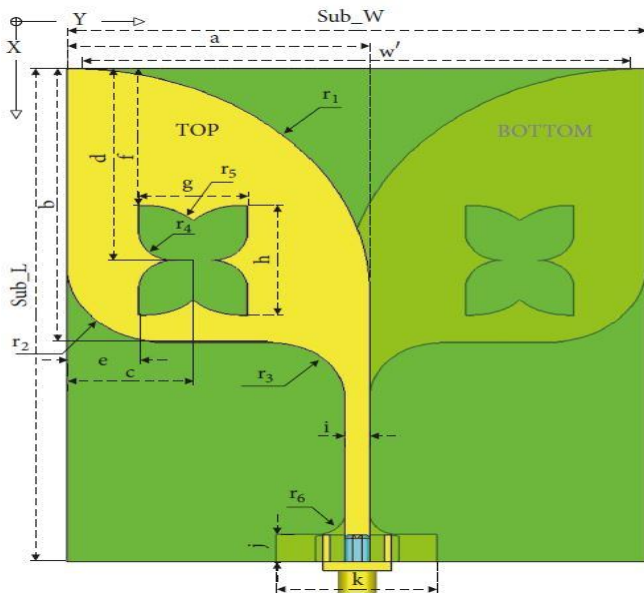
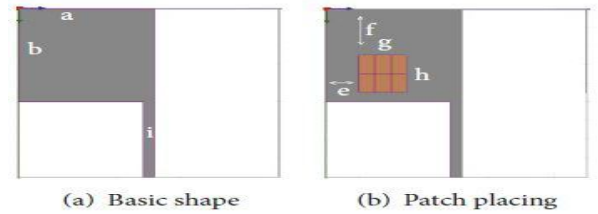


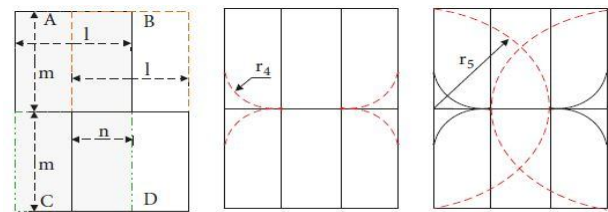
Figure 2: Designed structure of AVA with slots

The AVA should be designed in such manner that required overall impedance is obtained. An empirical method which is very studious procedure is done to meet required impedance. The flower type slot is made on the patch with fixed positions which is shown in figure 3(b), 3(c) and by proceeding the measurements given in the Table 1. As shown in figure 3(c) four Boxes A,B,C,D are initially positioned (f, e, Sub) , $(f, e+l/2, Sub)$, $(f+m, e, Sub)$, and $(f+m, e+l/2, Sub)$

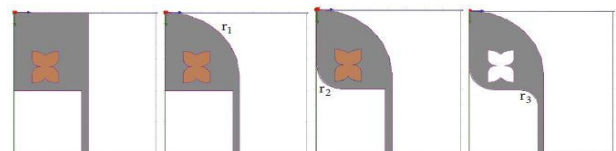
respectively. The bottom Boxes ABCD are consequently placed on the ground plane just by making *Sub* as zero $(f, e, 0)$, $(f, e+l/2, 0)$, $(f+m, e, 0)$, and $(f+m, e+l/2, 0)$ respectively. The shapes are appropriately constructed by using the procedural options like chamfer and union. The patch and ground has same type of slots with exponentially tapered edges with substrate in between.



(a) Basic shape (b) Patch placing



(c) Patch shaping progress



(d) AVA edges rounding to a final shape

Figure 3: Designed procedure of AVA structure

The design equations for the exponentially tapered edge are given by (1)–(3). These tapering edges are decided by opening rate *R*, r_1 and r_2 , where r_1 & r_2 are the radius of center of chamfer edges, which are defined by starting and ending points given by (x_1, y_1) and (x_2, y_2) respectively.

$$y = C_1 e^{Rx} + C_2 \tag{1}$$

Where C_1 & C_2

$$C_1 = \frac{y_1 - y_2}{e^{Rx_2} - e^{Rx_1}} \tag{2}$$

$$C_2 = \frac{y_2 e^{Rx_2} - y_1 e^{Rx_1}}{e^{Rx_2} - e^{Rx_1}} \tag{3}$$

The width of the opening of the flared edges w' is calculated by the cutoff frequency f_1 and the dielectric constant ϵ_r of substrate as given by below equation, Where value of c is given by 3×10^8 cm/sec (or) 30×10^8 mm/sec.

$$w' = \frac{c}{f_1 \sqrt{\epsilon_r}} \tag{4}$$

From the above equation considering the cutoff frequency as 2.2GHz and dielectric constant as 1.7 as the substrate used is denim jeans, width of flared edges is calculated as $w' = 78.5$ mm. The final prototype structure is designed, with widespread simulations and optimization process so that better and efficient results are achieved using HFSS. Final dimensions of designed AVA are tabulated in Table 1.

Table 1: Dimensions of Antenna

| | |
|------------------------|---------|
| <i>Sub_L</i> | 90.00mm |
| <i>Sub_W</i> | 80.00mm |
| <i>Sub_T</i> | 1.524mm |
| <i>a</i> | 41.75mm |
| <i>b</i> | 50.00mm |
| <i>c</i> | 17.50mm |
| <i>d</i> | 35.00mm |
| <i>e</i> | 10.00mm |
| <i>f</i> | 25.00mm |
| <i>g</i> | 15.00mm |
| <i>h</i> | 20.00mm |
| <i>i</i> | 03.50mm |
| <i>j</i> | 05.00mm |
| <i>k</i> | 22.00mm |
| <i>l</i> | 10.00mm |
| <i>m</i> | 10.00mm |
| <i>n</i> | 05.00mm |
| <i>w'</i> | 78.50mm |
| <i>r₁</i> | 41.00mm |
| <i>r₂</i> | 14.00mm |
| <i>r₃</i> | 10.00mm |
| <i>r₄</i> | 05.00mm |
| <i>r₅</i> | 09.00mm |
| <i>r₆</i> | 03.70mm |

3. ANTENNA DESIGN EVALUATION

In this section the performance of proposed antenna are analyzed and measured using HFSS. For the given design, HFSS software automatically generates a solution process and accurate mesh analysis. The antenna design-1 without slot and antenna design-2 with slots simulation results are compared to check superiority in design. Antenna design-1 works between the frequency range of 4.56GHz to 18.8GHz and antenna design-2 works between the ranges of 4GHz to more than 20GHz. So the proposed antenna successfully achieved ultra wide broadband. The important parameters duly considered for the analysis are namely Return loss (S_{11}), Gain, Radiation Pattern and VSWR are plotted for both antenna design-1 and antenna design-2.

3.1 Return Loss (S_{11}):

The attained return loss for the designed antenna-1 is shown in the figure 4 which is -24.3 dB at 7.07 GHz and -25.1 dB at 10.43 GHz and antenna design-2 shown in figure 8 which is -20.34dB at 12.4GHz, -30.61dB at 10.6GHz and -25.09dB at 6.9GHz. Return loss tells about how much power is being reflected by the port due to incident power.

3.2 Gain:

The term Antenna Gain describes how much power is transmitted in the direction of peak radiation to that of an isotropic source. The designed antenna is low power consuming since it has higher gain which is shown in three dimensional polar plot in figure 5. The gain of antenna design -1 is 6.31 dB at 7.07 GHz and 7.43 dB at 10.43 GHz and gain of antenna design-2 are 5.41dB, 6.82dB and 6.922dB with respect to 6.9GHz, 10.6GHz and 12.4GHz respectively as shown in figure 9. If an antenna's gain is 3 dB, it means that twice the amount of effective power will be sent in the direction of a target. Here, the gain is more than 3 dB which is appreciable value.

3.3 Radiation Pattern:

Radiation pattern (or) Antenna pattern (or) Far field pattern is the term used to represent the power radiated by antenna as a function of direction. A plot of gain as a function of direction is called radiation pattern is shown in figure 5 and figure 9 for antenna design-1 and antenna design-2 respectively.

3.4 VSWR:

The VSWR is defined as the amount of mismatch between antenna and the feeding line. The antenna design-1 has voltage standing wave ratio of 1.19 at 7.07 GHz and 1.21 at 10.43 GHz design and antenna design-2 of 1.06 for 12.4GHz.

4. GRAPHICAL REPRESENTATION OF SIMULATION RESULTS

The graphical representation of simulation results are shown below. Return loss S_{11} vs frequency is plotted which shows the operating frequency ($S_{11} < -10$ dB).

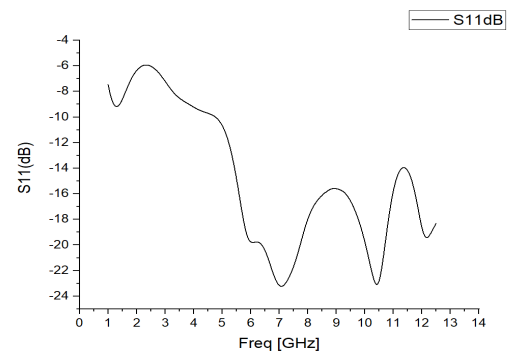


Figure 4: Frequency (GHz) vs Return loss (dB) antenna design -1

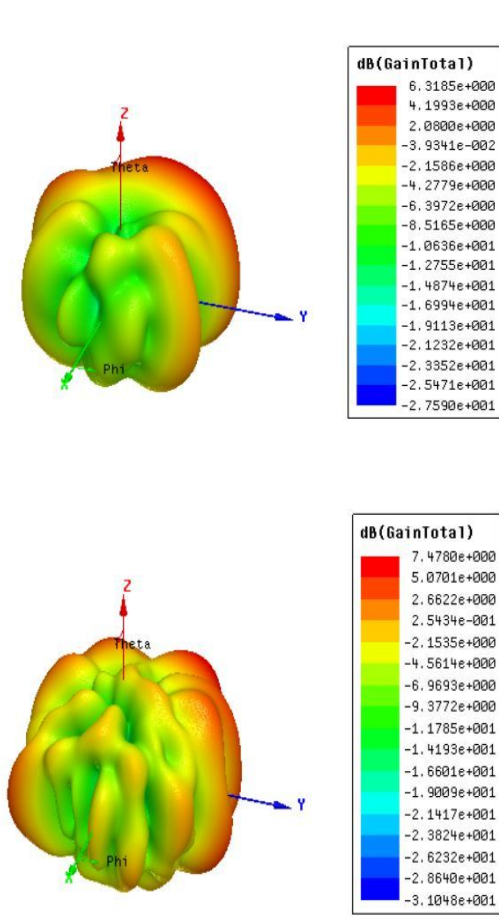


Figure 5: Gain of simulated antenna without slots in 3D view

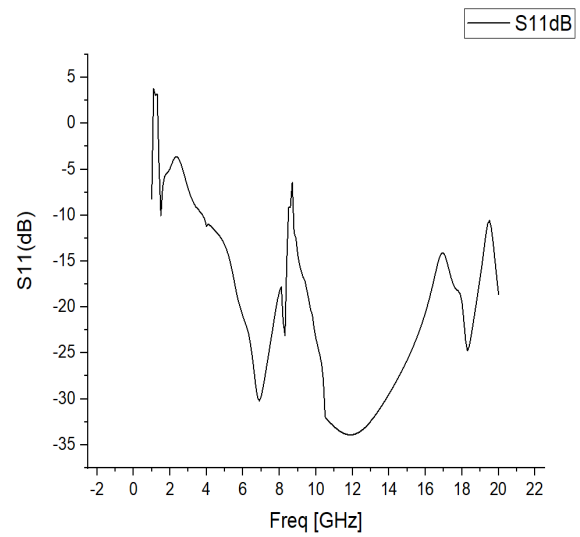


Figure 8: Frequency (GHz) vs return loss (dB) antenna design 2

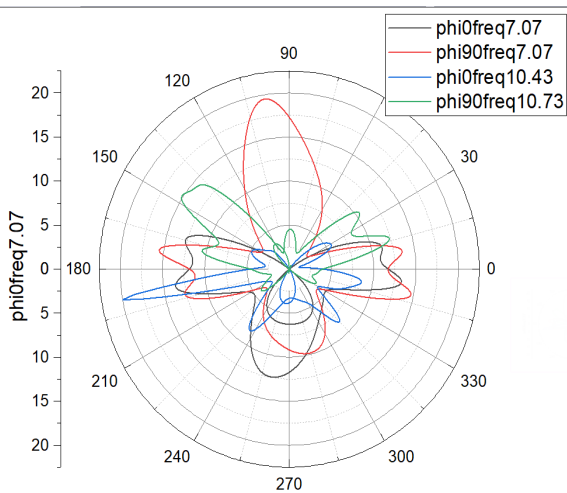
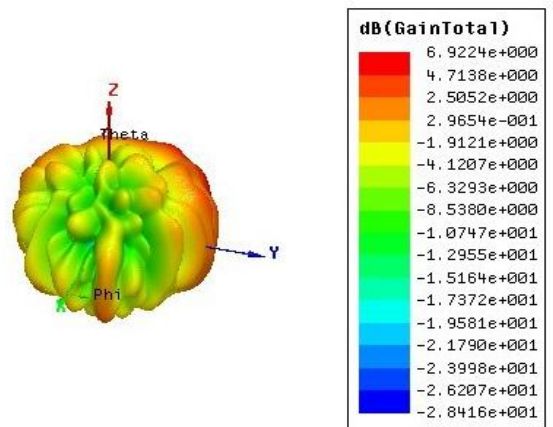
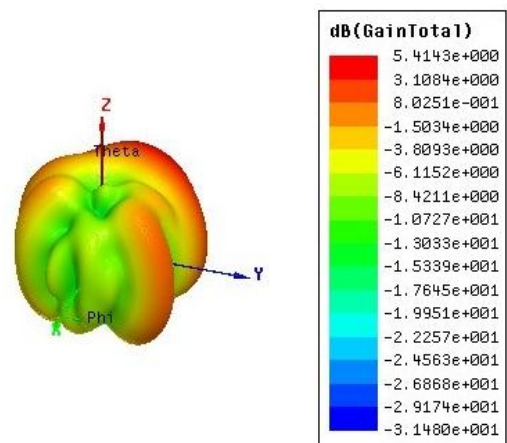


Figure 6: Overall radiation pattern of proposed antenna without slots.



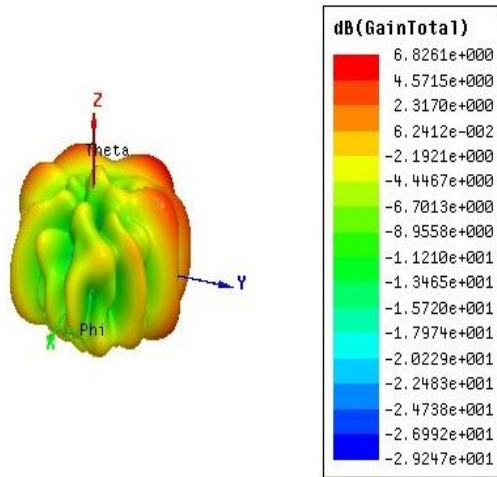


Figure 9: Gain of simulated antenna with slots in 3D view

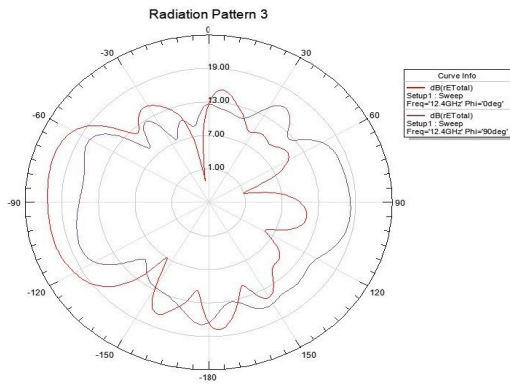
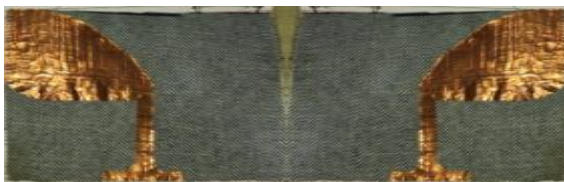


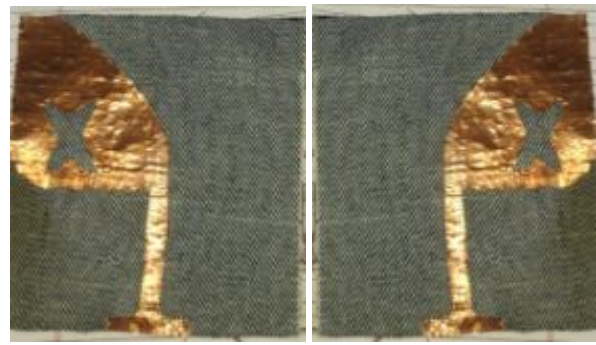
Figure 10: Overall radiation pattern of proposed antenna with slots

5. ANTENNA FABRICATION AND PRACTICAL MEASURED RESULTS

This section displays the fabricated antenna shown in figure 11(a,b,c,d) verifies the performance characteristics of fabricated antenna using network analyzer as shown in figure 12 and then tested fabricated antenna in anechoic chamber as shown in figure 13 and the results are compared with simulation results at 12.43GHz as given from figure 14 to figure 16.



(a) Without slot top view (b) Without slot bottom view



(c)With slot top view (d)With slot bottom view

Figure 11: Fabricated Antipodal Vivaldi Antenna



Figure 12: Testing AVA in Network Analyzer



Figure 13: Testing AVA in Anechoic Chamber

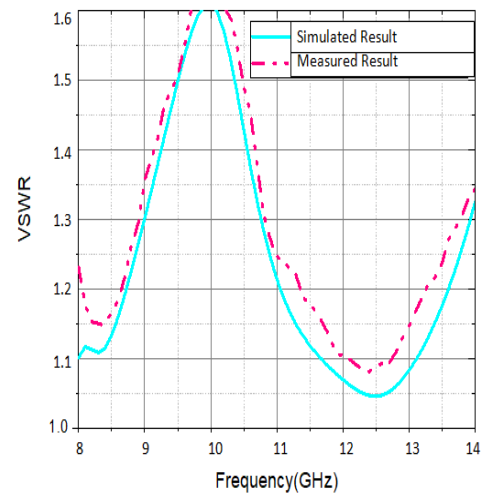


Figure 14: VSWR measured & simulated

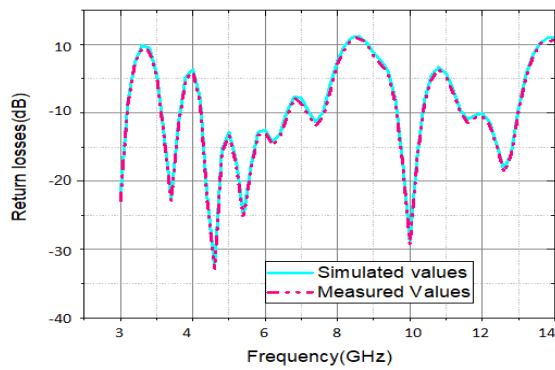


Figure 15: Return loss measured & simulated

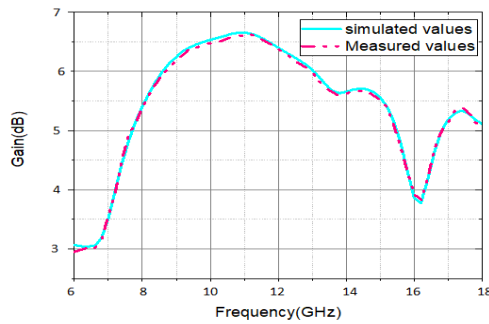


Figure 16: Gain measured & simulated

The following Table 2 compares performance characteristics the previous work done and present work done on Vivaldi Antennas and AVA for GPR applications.

Table 2: Previous and Present work done

| Ref | Frequency of Operation | Gain | Return loss (dB) | Substrate Material |
|--------------|---|------------|------------------|---|
| 25 | 0.7-2.1GHz | 1dB | -20 | FR4 $\epsilon_r=4.3$ and $\delta=0.025$ |
| 26 | 300 MHz to > 2GHz | 4.4-1.5dBi | -43 | Rogers RT/duroid 4350, $\epsilon_r=3.48, \delta=0.004$ |
| 27 | 1.5GHz | 2.83dB | -20 | FR4 $\epsilon_r=4.3$ and $\delta=0.025$ |
| 28 | 2GHz | 8.1dBi | -13 | FR4 $\epsilon_r=4.3$ and $\delta=0.025$ |
| 29 | 260-340 MHz(Vivaldi original) | 1.5dB | -13.2 | FR4 $\epsilon_r=4.4$ and $\delta=0.02$ |
| 30 | 220-282MHz(Vivaldi original 6 DGS) | 1.7dB | 13.2 | FR4 $\epsilon_r=4.4$ and $\delta=0.02$ |
| 31 | 220-263(Vivaldi original DGS) | 4.2dB | >22 | FR4 $\epsilon_r=4.4$ and $\delta=0.02$ |
| 32 | 7.52GHz | 15dBi | 13 | Rogers RT/duroid 5880, $\epsilon_r=2.2, \delta=0.0009$ |
| 33 | 6GHz | >3dB | >10 | Rogers RT/duroid 5870, $\epsilon_r=2.33, \delta=0.0012$ |
| Present Work | Vivaldi antenna without slot at 7.07GHz | 6.31dB | -24.3 | Denim Jeans $\epsilon_r=1.7$ and $\delta=0.025$ |
| | Vivaldi antenna without slot at 710.43GHz | 7.47dB | -25.12 | Denim Jeans $\epsilon_r=1.7$ and $\delta=0.025$ |
| | Vivaldi antenna with slot at 6.9GHz | 5.41dB | -25.09 | Denim Jeans $\epsilon_r=1.7$ and $\delta=0.025$ |
| | Vivaldi antenna with slot at 10.6GHz | 6.82dB | -30.61 | Denim Jeans $\epsilon_r=1.7$ and $\delta=0.025$ |
| | Vivaldi antenna with slot at 12.4GHz | 6.922dB | -20.34 | Denim Jeans $\epsilon_r=1.7$ and $\delta=0.025$ |

6. CONCLUSION

A high gain Anti-podal Vivaldi Antenna (AVA) has been proposed which can be used for microwave imaging, ground penetrating radar and radar applications. The AVA with flower slot and without slot structure is designed, simulated, fabricated and tested. The simulated results and practical results are very similar to each other. By comparing the two design models the antenna with slot is having better performance results than without slot in terms of bandwidth. Therefore, the proposed antenna design-1 has a bandwidth between 4.5GHz to 18.82GHz and antenna design-2 covers the ultra bandwidth range from 3.63GHz to greater than 20GHz with better VSWR and gain almost remains constant

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