

# Research the Length of the Braking Distance for Speed and High-Speed Trains on Railway Sections



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## ABSTRACT

The article provides a methodology for calculating the length of the braking distance on high-and high-speed sections of the railway of «UzbekistonTemirYollari» JSC. Method for calculating the length during emergency braking. According to the developed methodology, it is possible to determine information about the state of the input traffic light on a locomotive at a distance sufficient for emergency braking and, based on these calculations, develop technical measures to ensure unhindered train movement. The indication ahead of the traffic light in front of the vehicle is repeated in the cab of a locomotive driver when the train travels between two traffic lights or over a section of a given length near the floor signal. Information displayed about the permitted speed, taking into account all restrictions. It is also possible to display information about upcoming restrictions, braking distance, speed, etc. Based on static speed information, the on-board unit and floor unit calculate the braking speed curve. The system continuously displays the maximum permissible speed in the driver's cab, which is consistent with the following limit and therefore cannot be exceeded at the moment. This requires information about the distance to the next restriction. This information may be transmitted individually for a block section or standardized using a block section of a certain length. Unification of the length of block sections is justified only in case of predominantly homogeneous traffic, e.g. on specialized high-speed sections or suburban lines. The above expressions are used to analyze the automatic locomotive alarm system and determine the required length of the rail line. The optimum length of the rail coding line is determined and, based on the above expressions, an algorithm can be developed and programs can be drawn up taking into account the length of the braking distance

**Keywords:**braking distances, average unit braking force, locomotive slowdown, slowdown train

## 1.INTRODUCTION

In JSC "UzbekistonTemirYollari" on speed and high-speed sections of the railway equipped and not equipped with automatic blocking devices, for ensure the safety of train traffic with the use of traffic lights and without the use of traffic lights, use automatic locomotive signaling systems [12].

Currently in the systems of interval regulation of train traffic for improve the safety of train traffic, track devices of interval regulation are necessarily supplemented by automatic locomotive signaling systems, and in some cases they switch to regulation of train traffic without floor traffic lights, locomotive systems are becoming the main systems for regulating train traffic.

In a number of foreign countries: France, Germany, Spain, Italy, Sweden, the United States of America, etc. [1], [4], [5],[6], [7],[8], to increase the safety of train traffic on high-speed lines, train control systems have been developed and are being developed, such as the TVM 300/430, in which signal information is transmitted to the locomotive over the rail channel using frequency modulated signals, as well as through the laid along the rails plumes LZB - 80, 500, 700, 702.

## 2.METHODS

Since on the Uzbek railway it is envisaged to monitor the freedom of the haul using axle counters, then at the train approaches the station, a prerequisite is the transmission of information to the locomotive about the state of the input traffic light at a distance sufficient for emergency braking in the event of a closed state of the input traffic light. This distance can be determined by the following expression:

$$L_l = L_k + L_a + L_b \quad (1)$$

where:

$L_k$  is the distance traveled by the train from the moment the code signal is received by the automatic locomotive signaling devices;

$L_a$  is before the brake system of the train is activated;

$L_b$  is braking distance of the train from the beginning of braking.

The most common in practical use is the analytical method for calculating the stopping distance, based on the numerical integration of the train motion equation [2; 3] by speed intervals. By this case, the braking distance  $L_b$  in the calculations is taken to be equal to the sum of the preparatory path  $L_p$  (pre-brake), triggering of threshold elements  $L_{te}$  and valid path  $L_v$  of braking:

$$L_t = L_p + L_v + L_{te} \quad (2)$$

The division of the braking distance into  $L_p$  and  $L_a$  is purely conditional and is taken to simplify calculations in

the area of a transient mode of action of the braking force. It is accepted that during the time the train travels the pre-braking distance, the brakes in action haven't come yet, and by the end of the pre-braking distance, there is an instantaneous increase in the braking force to the maximum value, i.e., the braking force of the train does not increase gradually, and instantly, later some time, called preparation time. Such conditions correspond to the assumption, that filling the brake cylinders with air on the train occurs not by valid for each railway carriage, and after some time  $t_p$  called preparation time in all railway carriage simultaneously [8].

In expression (2)  $L_p$  is way, passable by train per the time preparation of brakes for action, m:

$$L_p = V_p \cdot t_p, \quad (3)$$

where  $t_p$  is time to prepare the brakes for action;

$$t_p = 20 - \frac{200i}{b_T}, \quad (4)$$

$i$  is slope of the path,  $i = -3\%$ ;

$b_T$  is average specific braking force, N/t;

$$b_T = 15000 \vartheta_{pncm} \varphi_{kp}. \quad (5)$$

$L_a$  is actual braking way, traversed by the train at maximum pressure in the brake cylinder;

$$L_a = \frac{\xi^{-1}}{2} \sum_{n+1}^n \frac{V_{n+1}^2 - V_n^2 - V_{n-1}^2}{b_T + w_0 + b_i}, \quad (6)$$

$V_{n+1}, V_n, V_{n-1}$  are initial and final speed in the accepted design interval, m/s;

$b_i = 10 * i$  is specific resistance to train movement from the slope of the track, N/t;

$w_0$  is main specific resistance to train movement, N/t;

$Q_j$  is part of the train mass attributable to wagons of a given type and downloads;

$\xi$  is strain deceleration, m/s, under the influence of a retarding force of 1 N/t;

$$\xi = \frac{\xi_L \bar{Q}_L + \xi_T Q_T}{\bar{Q}_L + Q_T}, \quad (7)$$

$\xi_L$  is locomotive deceleration, m/s

$\xi_T$  is deceleration of the train, m/s

$\bar{Q}_L$  is accounting mass of the locomotive, t [9]

$Q_T$  is strain mass, t

$$w_0 = \frac{w_0^I \bar{Q}_L \sum w_{0j}^I Q_j}{\bar{Q}_L \sum Q_j}, \quad (8)$$

$$w_0^I = 24 + 0.396V_a + 0.045V_a^2$$

$w_0^I$  is main specific resistance to movement of the locomotive, N/t

$V_a = V_n + V_{n+1}/2$  is average train speed in the selected interval, m/s;

$w_{0j}^I$  is main specific resistance to the movement of cars of this type, taking into account their actual load, N/t;

$$w_{0j}^I = 7 + \frac{30 + 3.6V_{cp} + 0.324V_{cp}^2}{q_0}, \quad (9)$$

$q_0$  is axial load, t;

$L_d$  is the distance traveled by the train after changing the signal indication on the locomotive devices.

If we take into account the cycle time of the code signal  $t_p = 1,7$  sec. and the transition from one signal indication to another then during this time the train will cover the distance:

$$L_d = V_n \cdot t_p \cdot 3$$

### 3.RESULTAND DISCUSSIONS

With considering into account the above, the length of the section of the approximations to the input traffic light and to the intersection of road and rail transport with considering into account the reliable braking and stopping of the train near of the input traffic light and near the level crossing is determined based on the presented mathematical expressions.

Algorithm developed and program compiled, which can be used for alert the locomotive driver and person on duty by station about the approach speed. In figure 1 proposed one of the block diagrams and in figure 2 research of the length of the braking distance for speed and high-speed trains.

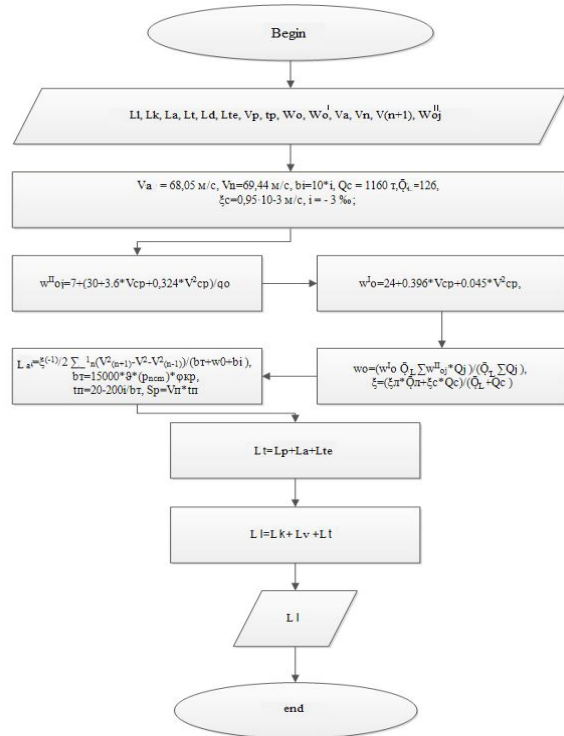


Figure 1:Block-scheme

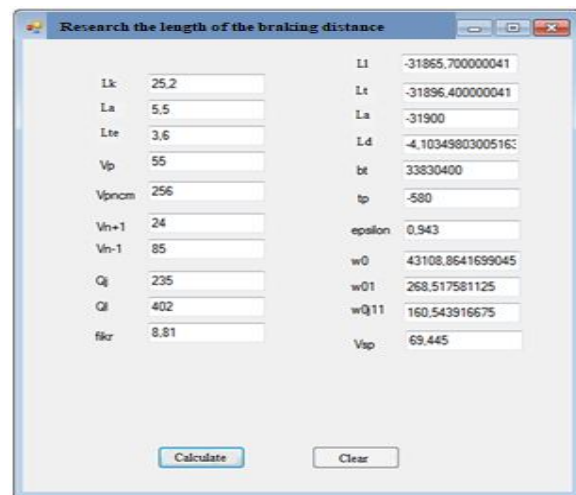


Figure 2:General view of the calculation using a computer program

The time it takes for the train to brake completely at the initial speed  $V_n$ , can be determined by the formula:

$$t = t_p + \sum_1^n \Delta t_V = t_p + t_V, \quad (10)$$

where  $t_p$  is time to prepare the brakes for action

$\Delta t_V$  is valid braking time;

$$\Delta t_V = \frac{\Delta L_a}{v_a}. \quad (11)$$

$\Delta L_a$  is actual braking way.

The quantity average deceleration is determined by the formula:

$$j = \frac{v_n - v_{n+1}}{\Delta t_V}. \quad (12)$$

#### 4. CONCLUSION

Based on all of the above, it is necessary to conduct research and determine the optimal section length of the approach, at which, under the locomotive's take-up coils be provided of the normative current of actuation of the devices automatic locomotive signaling.

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