

# Numerical Analysis of Flow Field in Vertical Wind Turbine at Free- Stream Turbulence Region

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## ABSTRACT

Air turbulence can affect the aerodynamic performance of wind turbines, and this effect is less on vertical wind turbines compared to horizontal wind turbines. In addition, vertical wind turbines have many advantages, but the literature related to their use to produce power is still small and needs to be developed. In this study, the effect of free-stream turbulence on the aerodynamic performance of Darrieus type vertical wind turbines was studied through two-dimensional numerical simulations. This performance can be observed through the power (P) and turbine power coefficient (C<sub>p</sub>). Simulations were carried out at 5% turbulent intensity (Tu) with variations in wind speed (U<sub>∞</sub>). The turbulent model used was the standard k-ε (SKE) and k-ω SST (SSTKW). The simulation results of the two turbulent models show the suitability for the power value (P) and the coefficient (C<sub>p</sub>) to the experimental results. The simulation result error reached 0.57% for C<sub>p</sub> with the standard k-ε turbulent model; 0.14% for C<sub>p</sub> with the k-ω SST model; 0.6% for P with the standard k-ε model; and 0.18% for P with the k-ω SST model.

**Keywords:** Wind turbine, Aerodynamics, Turbulence, Darrieus wind turbine.

## 1. INTRODUCTION

The aerodynamic performance of wind turbines can be affected by air turbulence. This performance can be shown from the wake turbine. The intensity of the turbine wake will decrease faster as turbulent intensity increases [1]. Furthermore, certain turbine wake characteristics can be a cause of power losses and increased fatigue loads in the turbine [2]. In addition to performance, air turbulence also affects loading on turbines [3], especially for horizontal wind turbines [4]. The effect of air turbulence is quite large for small scale wind turbines because the position of the turbine is closer to the ground. If the turbine is installed in a densely populated area, this position makes the turbine vulnerable to obstacles such as buildings or trees [5] which can disrupt air

flow in the turbine rotor. This barrier raises the potential for higher turbulent intensity compared to turbines in quiet areas of the population [6].

Vertical axis wind turbines (VAWT) have several advantages compared to horizontal wind turbines, namely the structure is more balanced, less noisy, easier to adjust to architectural design [7], compact design, easily connected with gears or generators, easier blade control, and low levels of fatigue [8]. With these advantages, vertical axis wind turbines have the potential to continue to be utilized.

Research on power utilization in vertical wind turbines has not been done much. The usual approach to obtain power curves is to determine the output power by averaging the measured power from wind speed [9], but this method does not include the free-stream turbulence effect. In a study conducted by Kooiman and Tullis [10], vertical wind turbines were tested for energy production based on the influence of air velocity and changes in flow direction without the control of free-stream turbulence levels. The results obtained that the turbine output power varies with changes in speed, but independent of changes in direction. Output data in this study are divided into data groups, each data group is determined turbulent intensity and aerodynamic characteristics. This approach is very dependent on the output data sample size, so it is possible to obtain different results if the data sample size is different.

Based on research conducted by Kooiman and Tullis [10], testing with turbulent flow control is needed. Detailed analysis in the turbulence-free stream area around the vertical turbine blade is scarce. Therefore, this study aims to look at the effect of the intensity of free-stream turbulence on the aerodynamic performance of Darrieus type vertical wind turbines through two-dimensional numerical simulations. Some numerical investigations in various application have been reported by researchers [11-13]

## 2. PHYSICAL MODEL

Simulations in this study refer to experiments conducted by Baloutaki, Carriveau, and Ting [14]. They conducted a vertical wind turbine type Darrieus experiment in an air column with a turbulent generator to see the effect of free-stream turbulence on turbine aerodynamic performance. The length of the tested air column is 1.8 m. The size of the air column cross-section is 0.76 m x 0.76 m. Simulations were carried out on a small vertical wind turbine, model P10, produced by Shanghai Aeolus Windpower Technology Co., Ltd. (SAWT) [15]. This Darrieus type of wind turbine has five blades and is made of aluminum, as shown in Figure 1. These wind turbine blades have a custom airfoil profile. The coordinates of this airfoil profile are shown in Figure 2. The length of the blade chord and turbine height are 45 mm and 0.3 m, respectively. The diameter of the turbine rotor is 0.3 m. Each turbine blade is connected with a rotary shaft through two supporting rods at position 0.33 and 0.66 of the turbine height. Supporting rods made of aluminum with a square cross-section with a size of 2 mm x 25 mm.



Figure 1 : Vertical wind turbine, model P10 (SAWT).

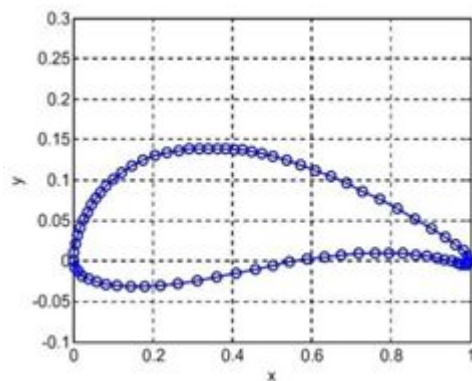


Figure 2 : Airfoil profile [14].

## 3. MATHEMATICAL MODEL

### 3.1 Governing Equations

The flow field around the vertical wind turbine has asymmetric, periodic, unsteady, separated, and turbulent

characteristics [14]. The fluid flow builder equation represents the equation of conservation of mass, momentum, and energy [16]. The equation for the conservation of mass is shown in Eq. 1 [17]

$$\frac{\partial \rho}{\partial t} + \frac{\partial(\rho u)}{\partial x} + \frac{\partial(\rho v)}{\partial y} + \frac{\partial(\rho w)}{\partial z} = 0 \quad (1)$$

Eq. (1) is a three-dimensional mass conservation equation or continuity equation under compressible fluid conditions. This equation consists of two compilers on the left side, namely the rate of change in density with respect to time and mass flow rate out of control volume. In this study, the air is assumed to be incompressible, and simulations are carried out in the XY plane, then Eq. (1) becomes Eq. (2).  $u$ ,  $v$ , and  $w$  are velocity vectors.

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \quad (2)$$

The conservation of momentum equation for the  $x$  and  $y$  directions is shown in Eq. 3 and 4. The equation for the  $z$ -direction is not discussed because this study reviews the flow only in the XY plane. The left side of these equations shows the rate of increase in momentum per unit volume in the  $x$  and  $y$  directions.  $S_{Mx}$  and  $S_{My}$  are source terms such as body force caused by gravity. The energy conservation equation will not be discussed because, in this study, the temperature difference is very small.

For the standard  $k-\epsilon$  turbulent model (SKE), the turbulent kinetic energy ( $k$ ) and turbulent dissipation rate ( $\epsilon$ ) are obtained from the transfer Eq. (5) and Eq.(6) [18].  $G_k$  represents the formation of turbulent kinetic energy due to the average velocity gradient.  $G_b$  represents the formation of turbulent kinetic energy due to buoyancy. Buoyancy is a state characterized by the presence of non-zero gravitational fields and temperature gradients simultaneously.

In Eq.8,  $Prt$  is a turbulent Prandtl number for energy and  $g_i$  is a component of the gravity vector in the  $i$ -th direction. For the SKE turbulent model, the default value of  $Prt$  is 0.85.  $\beta$  is the coefficient of thermal expansion. The degree showing the effect of buoyancy on  $\epsilon$  is determined by the constant  $C3\epsilon$ . In Eq. 10,  $v$  and  $u$  are components of flow velocity that are parallel to and perpendicular to the gravity vector.  $Y_M$  is dilatation dissipation.  $M_t$  is a turbulent Mach number. In Eq. (12),  $a$  is the speed of sound.  $\sigma_k$  and  $\sigma_\epsilon$  are turbulent Prandtl numbers for  $k$  and  $\epsilon$ , respectively.  $S_k$  and  $S_\epsilon$  are user-defined source terms.  $\mu_t$  is turbulent (eddy) viscosity. The default values for  $C1\epsilon$ ,  $C2\epsilon$ ,  $C_\mu$ ,  $\sigma_k$ , and  $\sigma_\epsilon$  are 1.44; 1.92; 0.09; 1; and 1.3, respectively.

$$\rho \frac{DU}{Dt} = \frac{\partial(-\rho + T_{xx})}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial T_{xx}}{\partial z} + S_{Mx} \quad (3)$$

$$\rho \frac{\partial v}{\partial t} = \frac{\partial \tau_{xy}}{\partial x} + \frac{\partial (-p + \tau_{yy})}{\partial y} + \frac{\partial \tau_{zy}}{\partial z} + S_{My} \quad (4)$$

$$\begin{aligned} \frac{\partial}{\partial t}(\rho k) + \frac{\partial}{\partial x_i}(\rho k u_i) = \\ \frac{\partial}{\partial x_j} \left[ \left( \mu + \frac{\mu_t}{\sigma_k} \right) \frac{\partial k}{\partial x_j} \right] + G_k + G_b - \rho \varepsilon - Y_M + S_k \end{aligned} \quad (5)$$

$$\begin{aligned} \frac{\partial}{\partial t}(\rho \varepsilon) + \frac{\partial}{\partial x_i}(\rho \varepsilon u_i) = \\ \frac{\partial}{\partial x_j} \left[ \left( \mu + \frac{\mu_t}{\sigma_\varepsilon} \right) \frac{\partial \varepsilon}{\partial x_j} \right] + C_{1\varepsilon} \frac{\varepsilon}{k} (G_k + C_{3\varepsilon} G_b) - C_{2\varepsilon} \rho \frac{\varepsilon^2}{k} + S_\varepsilon \end{aligned} \quad (6)$$

$$G_k = -\rho u_i' u_j' \frac{\partial u_j}{\partial x_i} \quad (7)$$

$$G_b = \beta g_i \frac{\mu_t}{\rho \Gamma_i} \frac{\partial T}{\partial x_i} \quad (8)$$

$$\beta = -\frac{1}{\rho} \left( \frac{\partial \rho}{\partial T} \right)_p \quad (9)$$

$$C_{3\varepsilon} = \tanh \left| \frac{v}{u} \right| \quad (10)$$

$$Y_M = 2\rho \varepsilon M_{T0}^2 \quad (11)$$

$$M_T = \sqrt{\frac{k}{a^2}} \quad (12)$$

$$a = \sqrt{\gamma RT} \quad (13)$$

$$\mu_t = \rho C_\mu \frac{k^2}{\varepsilon} \quad (14)$$

For the turbulent model k- $\omega$  SST (SSTKW), the turbulent kinetic energy (k) and the specific turbulent dissipation rate ( $\omega$ ) are obtained from the transfer Eq.15 and Eq. (16) [18].  $G\omega$  represents formation  $\omega$ . The value of  $R\omega$  is 2.95.  $\Gamma_k$  and  $\Gamma\omega$  are effective diffusivity k and  $\omega$ .  $Y_k$  and  $Y\omega$  are dissipation k and  $\omega$  due to turbulence. Values  $\zeta^*$ ,  $R\beta$ , and  $\beta\infty^*$  are 1.5; 8; and 0.09. The value of  $M_{T0}$  is 0.25.  $D\omega$  is cross-diffusion. In Eq. 24, S is the strain rate.  $F_1$  and  $F_2$  are blending functions. In Eq. 28, y is the distance to the surface and  $D\omega^+$  is the positive part of cross-diffusion.

$$\frac{\partial}{\partial t}(\rho k) + \frac{\partial}{\partial x_i}(\rho k u_i) = \frac{\partial}{\partial x_j} \left( \Gamma_k \frac{\partial k}{\partial x_j} \right) + G_k - Y_k + S_k \quad (15)$$

$$\frac{\partial}{\partial t}(\rho \omega) + \frac{\partial}{\partial x_j}(\rho \omega u_j) = \frac{\partial}{\partial x_j} \left( \Gamma_\omega \frac{\partial \omega}{\partial x_j} \right) + G_\omega - Y_\omega + D_\omega + S_\omega \quad (16)$$

$$G_\omega = \frac{\sigma}{\nu_i} G_k \quad (17)$$

$$\alpha = \frac{\alpha_\infty}{\alpha^*} \left( \frac{\alpha_\Omega + R\beta\varepsilon/R\omega}{1 + R\beta\varepsilon/R\omega} \right) \quad (18)$$

$$\alpha^* = \alpha_\infty^* \left( \frac{\alpha_\Omega + R\beta\varepsilon/R_k}{1 + R\beta\varepsilon/R_k} \right) \quad (19)$$

$$R\beta\varepsilon = \frac{\rho k}{\mu\omega} \quad (20)$$

$$\alpha_\Omega^* = \frac{\beta_i}{\alpha} \quad (21)$$

$$\Gamma_k = \mu + \frac{\mu_t}{\sigma_k} \quad (22)$$

$$\Gamma_\omega = \mu + \frac{\mu_t}{\sigma_\omega} \quad (23)$$

$$\mu_t = \frac{\rho k}{\omega} \frac{1}{\max \left[ \frac{1}{\kappa^2 y^2}, \frac{1}{\omega} \right]} \quad (24)$$

$$\sigma_k = \frac{1}{F_{k,1} + (1 - F_{k,1})/\sigma_{k,2}} \quad (25)$$

$$\sigma_\omega = \frac{1}{F_{\omega,1} + (1 - F_{\omega,1})/\sigma_{\omega,2}} \quad (26)$$

$$F_i \tanh(\Phi_i^{-4}) \quad (27)$$

$$\Phi_1 = \min \left[ \max \left( \frac{\sqrt{k}}{0.09\omega y}, \frac{500\mu}{\rho y^2 \omega} \right), \frac{4\rho k}{\sigma_{\omega,2} D\omega^+ y^2} \right] \quad (28)$$

$$D\omega^+ = \max \left[ 2\rho \frac{1}{\sigma_{\omega,2}} \frac{1}{\omega} \frac{\partial k}{\partial x_j} \frac{\partial \omega}{\partial x_j}, 10^{-10} \right] \quad (29)$$

$$F_2 = \tanh(\Phi_2^2) \quad (30)$$

$$\Phi_2 = \max \left[ 2 \frac{\sqrt{k}}{0.09\omega y}, \frac{500\mu}{\rho y^2 \omega} \right] \quad (31)$$

$$Y_k = \rho \beta^* k \omega \quad (32)$$

$$\beta^* = \beta_i^* [1 + \zeta^* F(M_T)] \quad (33)$$

$$Y_\omega = \rho \beta \omega^2 \quad (34)$$

$$\beta = \beta_i \left[ 1 - \frac{\beta_i}{\beta_i} \zeta^* F(M_T) \right] \quad (35)$$

$$\beta_i^* = \beta_\infty^* \left( \frac{\frac{4}{15} + (R\beta\varepsilon/R\omega)^{0.75}}{1 + (R\beta\varepsilon/R\omega)^{0.75}} \right) \quad (36)$$

$$F(M_T) = \begin{cases} 0 & M_T \leq M_{T0} \\ M_T^2 - M_{T0}^2 & M_T > M_{T0} \end{cases} \quad (37)$$

$$M_T^2 \equiv \frac{2k}{a^2} \quad (38)$$

$$\beta_i = F_1 \beta_{i,1} + (1 - F_1) \beta_{i,2} \quad (39)$$

### 3.2 Boundary conditions

In this two-dimensional simulation, the computational domain boundary conditions consist of velocity inlet, outlet pressure, wall, and symmetry. The boundary conditions in the computational domain are shown in Eq. (40), (41) and (42). The values of wind speed, turbine rotational speed, power, and power coefficient used in the simulation are shown in Table 1. The computational domain is divided into three sub-domains, namely, sub-domains A, B, and C (see Figure 5). Sub-domain B is organized as moving mesh, while sub-domains A and C are managed as stationary mesh. The turbine blade surface was set as a non-slip wall. Simulations were carried out at a turbulent intensity (Tu) of 5%. The turbulent model used was the standard k-ε (SKE) and k-ω SST (SSTKW).

$$\text{Inlet} \quad \mathbf{u} = U_{\infty}, \mathbf{v} = 0 \quad (40)$$

$$\text{Outlet} \quad P = P_{atm} \quad (41)$$

$$\text{Wall} \quad \mathbf{u} = \mathbf{v} = 0 \quad (42)$$

### 4. NUMERICAL METHOD

Mesh in the computational domain was divided into moving mesh in the area around the turbine blade and stationary mesh in the inside and outside of the turbine. The mesh was reduced in the area around the blade and inside the turbine. Figure 3 shows the overall mesh detail. Figure 4 shows the mesh around the turbine blade. The mesh used was a hybrid mesh consisting of structured and triangle mesh, as shown in Figure 7. The hybrid mesh is a type of mesh that is good in terms of accuracy and automation [19]. The number of mesh was 958124 cells.

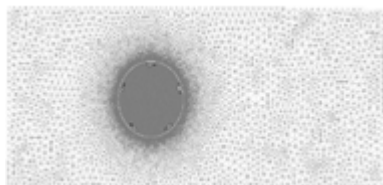


Figure 3: Mesh of the whole computational domain



Figure 4: Mesh around the turbine blade

Table 1: Data on wind speed, turbine rotational speed, power, and power coefficient [14].

No.	$U_{\infty}$ (m/s)	$n$ (rpm)	$P$ (Watt)	$\lambda$	$C_p$
1	3.0441	13.8495	0.0227	0.0714	0.0002
2	3.4125	21.1520	0.0227	0.0973	0.0002
3	3.7809	28.2027	0.0227	0.1171	0.0005
4	4.1929	33.2389	0.0227	0.1245	0.0009
5	4.4256	35.5052	0.0227	0.1260	0.0009
6	4.8861	42.8077	0.0227	0.1375	0.0012
7	5.2109	49.8584	0.0202	0.1502	0.0014
8	5.4823	57.1608	0.0227	0.1637	0.0021
9	5.9476	66.7296	0.0454	0.1761	0.0026
10	6.4033	81.3346	0.0681	0.1994	0.0035
11	6.7765	90.6516	0.0681	0.2100	0.0040
12	7.1013	112.3072	0.1159	0.2483	0.0061
13	7.5133	167.4536	0.2848	0.3499	0.0124
14	7.7896	191.3755	0.3831	0.3857	0.0152
15	8.1580	220.3336	0.5495	0.4240	0.0185
16	8.6670	310.9852	1.3182	0.5633	0.0376
17	9.0354	335.1590	1.6736	0.5824	0.0426
18	9.3553	351.7784	2.0844	0.5904	0.0475
19	9.6801	392.5716	2.6112	0.6367	0.0538
20	9.9127	435.8829	3.2565	0.6904	0.0624
21	10.4169	483.7268	4.0252	0.7291	0.0667
22	10.8337	526.7863	4.7889	0.7634	0.0704
23	11.1537	558.0107	5.3888	0.7855	0.0730
24	11.5221	586.7170	5.9382	0.7995	0.0728
25	11.8905	615.4234	6.6087	0.8126	0.0735
26	12.2637	646.6478	7.2791	0.8278	0.0739

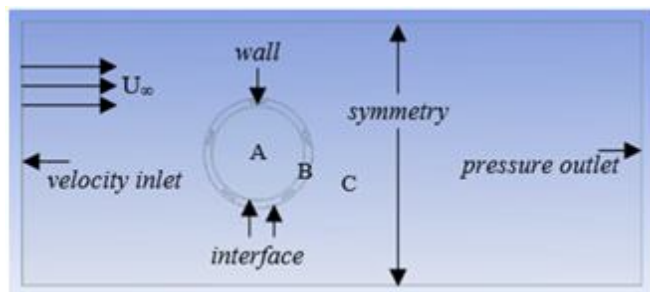


Figure 5: Computational domain and boundary conditions.

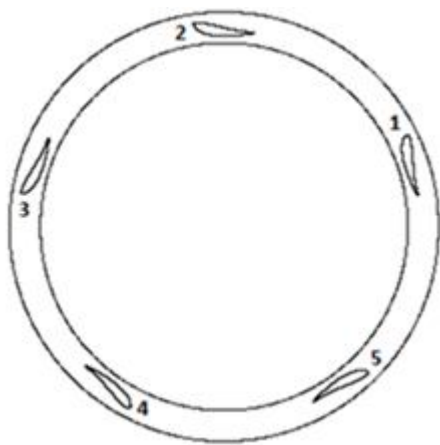


Figure 6: Position number of turbine blade

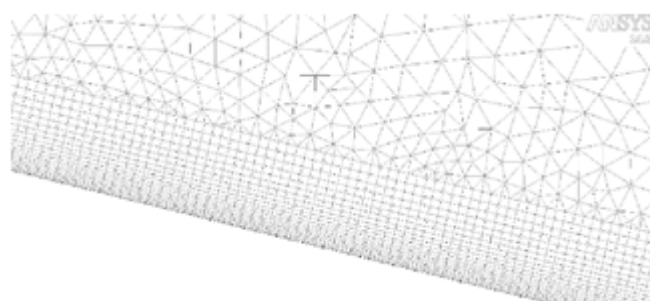


Figure 7: Mesh detail around the turbine blade surfaces

Some amount of mesh has been tested to obtain an independent mesh. Independent mesh indicates that the addition of the next mesh number no longer influences the simulation results. From the results of mesh testing, independent mesh has a total of 958124 elements.

The spatial discretization used is the second-order upwind for the momentum equation, the first order upwind for the turbulent equation, the least-squares cell-based for the gradient, and the standard for pressure. The pressure-velocity coupling used is SIMPLEC (Semi Implicit Method for Pressure Linked Equations Consistent). The iteration process residue is set to 0.0001 for the equation of continuity, momentum, and turbulence.

## 4. RESULT AND DISCUSSION

### 4.1 Validation

The numerical simulation results of this study were validated with experimental data conducted by Baloutaki, Carriveau, and Ting [14]. The parameters compared are turbine power and power coefficient. The turbine power coefficient was calculated by Eq. (43) [20]. Turbine power was calculated by Eq. (44) [21].  $C_m$  is the moment coefficient obtained from the iteration results.  $\lambda$  is the tip speed ratio.  $\lambda$  shows the ratio between turbine rotational speed and free-stream airspeed, see Eq. (45) [22].  $\rho$  is the density of air,  $R$  is the radius of the turbine rotor,  $h$  is the height of the turbine rotor.

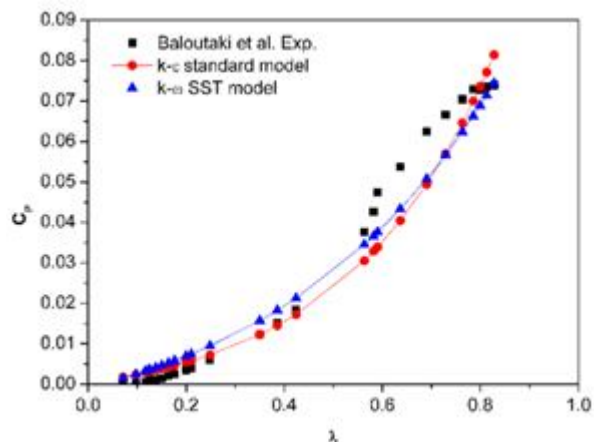
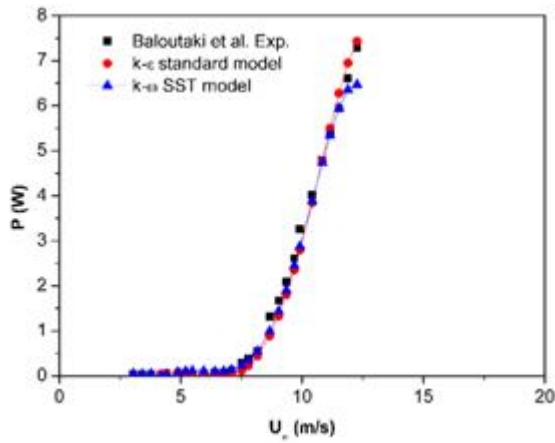


Figure 8: Comparison of turbine power coefficient between simulation and experiment Comparison of turbine power coefficient between simulation and experiment

Figures 8 and 9 show that the simulation results of the two turbulent models have the same tendency in increasing  $C_P$  and  $P$ . Simulation of wind turbines with CFD is usually done at transient conditions to see transient effects [22]. The simulation in this study was carried out on a steady-state to observe the results of  $C_P$  and  $P$  wind turbines. The results showed that the simulation on the steady-state for wind turbines was not good.

The results showed a match between the results of simulations and experiments for several values of tip speed ratio. In some tip speed ratios, the power simulation results and the power coefficient exceed the experimental results, and this is due to the limitations of two-dimensional modeling [23, 24]. Besides, this excess power and coefficient of power are also due to the use of a fully turbulent RANS (Reynolds Average Navier-Stokes) model for low Reynolds numbers [25]. Two-dimensional modeling does not take into account three-dimensional effects such as vortex tips and irregular pressure distribution on three-dimensional blades.



**Figure 9:** Comparison of turbine power between simulation and experiment.

$$C_P = C_m \times \lambda \tag{43}$$

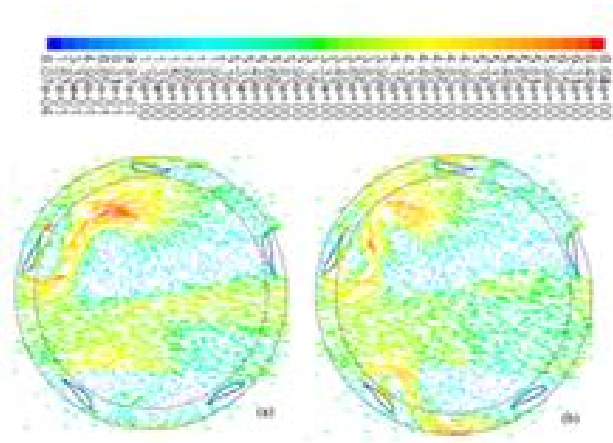
$$P = \frac{1}{2} \times \rho \times (U_{\infty}^3) \times 2 \times R \times h \times C_P \tag{44}$$

$$\lambda = \frac{R\omega}{U_{\infty}} \tag{45}$$

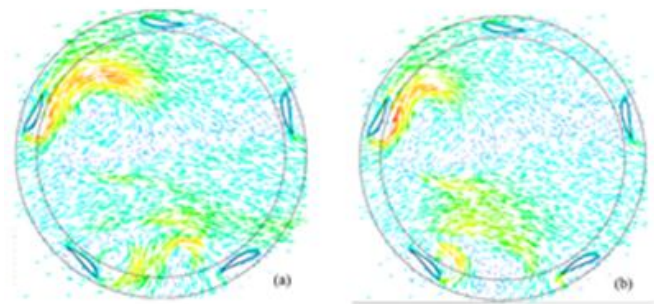
#### 4.2 Velocity Field Distribution

The parameters observed from the simulation results are the distribution of speed, turbulent kinetic energy, and pressure in the area around the turbine rotor. Figures 10 and 11 show the velocity vector distribution of the simulation results of the turbulent model k-ε standard and k-ω SST at wind speeds of 3.04 and 12.26 m/s. The figure shows the vortex formed in the wake blade area 3 and 4, both at low and high free-stream speeds. The greater the angle of attack, the boundary layer will be more difficult to continue to stick to the surface of the airfoil, and the separation area will be even greater [26]. This flow separation causes vortex [27].

At free-stream speeds of 3.04 m / s, the number of vortices formed each pair in the wake area of blades 3 and 4. Each pair of vortices has the opposite direction. This is consistent with research conducted by Fujisawa and Shibuya [28]. However, the two pairs of the vortex have different shapes between the two turbulent models. In the standard k-ε turbulent model, the larger vortex in the wake blade 3 area looks closer to the center of the turbine. Whereas on blade 4, the vortex that is closer to the surface of the blade appears to be stretching. In the k-ST SST model, the larger vortex in the wake blade three areas is seen moving away from the center of the turbine.



**Figure 10:** Velocity vector (m/s) at U = 3.04 m/s. (a) standard k- ε , (b) k-ω SST



**Figure 11:** Velocity vector (m/s) at U = 12.26 m/s. (a) standard k- ε , (b) k-ω SST

At a free-stream speed of 12.26 m/s, the vortex pair in the wake blade 3 area gets closer to the blade so that it appears that one of the vortices, which is a smaller vortex, has decreased in size due to the insistence of a larger vortex. The closer the vortex pair to blade 3, causing the interaction of the blade-vortex, which causes an increase in wind turbine power [28]. The vortex pair in the wake blade three regions also appears to have a different shape between the two turbulent models. One vortex closer to the center of the turbine appears larger on the standard k-ε model than k-ω SST. On wake blade 4, the standard k-ε model shows more vortices than the k-ω SST model.

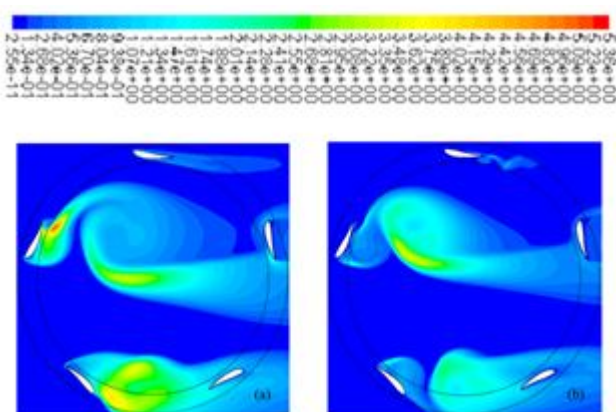
It can be said that the formation of vortex is influenced by free-stream speed, or in other words, is influenced by tip speed ratio. The velocity vector results also show different flow conditions at each blade.

In the area inside the turbine, the same two turbulent models show a decrease in speed, both at 3.04 and 12.26 m/s free-stream speed. This is consistent with research conducted by Guilherme Silva [29]. This decrease in speed is clearly

seen in the wake area of the turbine blade, which is shown in blue. This decrease in speed indicates that the simulation results are in accordance with existing physical phenomena.

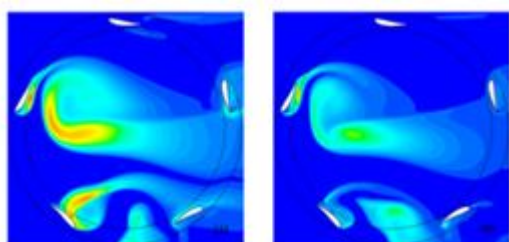
### 4.3 Turbulent Kinetic Energy Distribution

The distribution of turbulent kinetic energy around the turbine rotor is shown in Figures 12 and 13. Figure 12 shows the turbulent kinetic energy contours of the two turbulent models at wind speeds of 3.04 m / s. Figure 13 shows the turbulent kinetic energy contour at a wind speed of 12.26 m / s. This contour shows that each blade produces different turbulent levels. This turbulence then carries along the wake that is generated until it slowly disappears. This shows that the eddy structure in the flow is gradually anticipated [30].



**Figure 12:** Turbulent kinetic energy contours ( $m^2/s^2$ ) at  $U = 3.04$  m/s. (a) standard  $k-\epsilon$  , (b)  $k-\omega$  SST.

Areas with high turbulent kinetic energy indicate complex turbulent flow such as slip flow [30]. Turbulent kinetic energy contours in the turbine sweep area increase with increasing turbine rotational speed. This shows that the turbine rotational speed has an influence on the flow field structure [30].

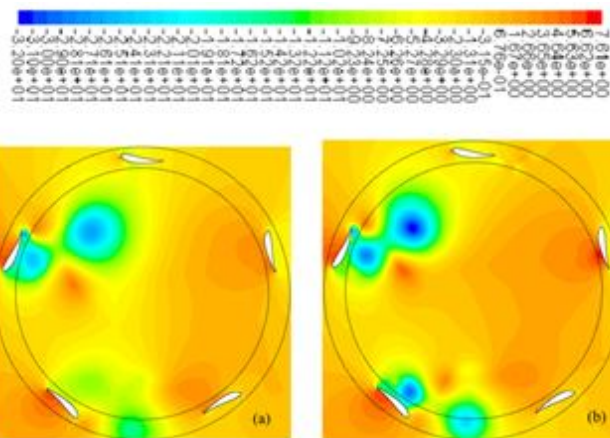


**Figure 13:** Turbulent kinetic energy contours ( $m^2/s^2$ ) at  $U = 12.26$  m/s. (a) standard  $k-\epsilon$  , (b)  $k-\omega$  SST

### 4.4 Pressure Distribution

The distribution of pressure around the turbine rotor is shown in Figures 14 and 15. Figure 14 shows the pressure contours

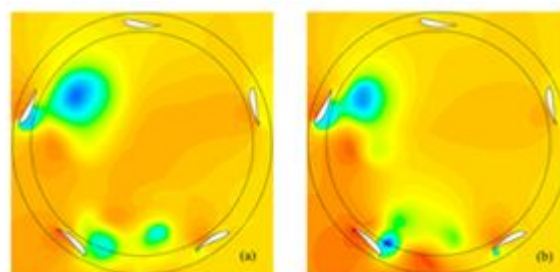
of the two turbulent models at a wind speed of 3.04 m/s. Figure 15 shows the pressure contour at a wind speed of 12.26 m/s. Pressure drops around the rotor are clearly visible on blades 3 and 4, shown in blue in the waking area. This pressure drop occurs because of the transfer of energy to the turbine blade [31] so that it is converted to power [32].



**Figure 14:** Pressure contour (Pa) at  $U = 3.04$  m/s. (a) standard  $k-\epsilon$  , (b)  $k-\omega$  SST.

The region with high pressure is located on the upstream blade, while areas with lower pressure are located on the downstream blade. The low-pressure region in the wake blade 3 and 4 has a correlation with the high-speed vortex shown in Figures 10 and 11. This shows the suitability between the velocity and pressure distribution.

Pressure distribution indicates the area with non-uniform pressure in the path of the turbine blade and the blade facing the direction of flow [31]. This pressure greatly contributes to the torque produced. A high-pressure area on the side of the turbine blade facing the direction of flow will increase turbine rotation, which contributes to increase torque.



**Figure 15:** Pressure contour (Pa) at  $U = 12.26$  m/s. (a) standard  $k-\epsilon$  , (b)  $k-\omega$  SST.

## 5. CONCLUSION

In this research, a two-dimensional simulation of a Darrieus type vertical wind turbine was carried out under steady conditions to observe the performance of a wind turbine,

namely CP and P. To approach the actual physical condition of the turbine, the computational domain used a moving mesh in the area around the turbine blade. Independent mesh was obtained after the mesh testing process several times.

The simulation results using the turbulent model k-ε standard and k-ω SST showed compatibility with CP and P experiments. But on some tip speed ratio values, the CP and P values exceed the experimental results, and this was due to the limitations of two-dimensional modeling that does not take into account three-dimensional effects such as tip vortex. So the authors suggest applying three-dimensional modeling for the case of wind turbines in further research.

The observed flow field included the distribution of velocity, turbulent kinetic energy, and pressure. The distribution of velocity vectors showed the presence of vortices that are in accordance with previous studies and proves that vortex formation was affected by the tip speed ratio. Turbulent kinetic energy distribution successfully showed the influence of turbine rotational speed on turbulent kinetic energy. Likewise, the distribution of stresses can indicate actual physical phenomena.

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#### NOMENCLATURE

u x-axis velocity vector  
 v y-axis velocity vector  
 w z-axis velocity vector  
 Tu turbulent intensity  
 U∞ turbulence free-stream velocity  
 k turbulent kinetic energy  
 ε turbulent dissipation rate  
 Gk the formation of k due to the average velocity gradient  
 Gb the formation of k due to buoyancy  
 Prt turbulent Prandtl numbers for energy  
 gi the gravity vector component in the i-direction  
 β coefficient of thermal expansion  
 C3ε degree of influence of buoyancy on ε  
 YM dilated dissipation  
 Mt turbulent Mach numbers  
 a speed of sound  
 σk Prandtl number for k  
 σε Prandtl numbers for ε  
 Sk user-defined source term for k  
 Σε user-defined source term for ε  
 μt turbulent viscosity  
 ω turbulent specific dissipation rate

Gω formation of ω  
 Γk effective diffusivity k  
 Γω effective diffusivity ω  
 Yk dissipation k due to turbulence  
 Yω dissipation ω due to turbulence  
 Dω cross diffusion  
 S strain rate  
 F1, F2 blending function  
 y distance to the surface  
 Dω+ positive part of cross diffusion  
 p outlet pressure  
 n turbine rotational speed  
 P turbine power  
 $P=0,5 \times \rho \times ([U_{\infty}]^3) \times 2 \times R \times h \times C_P$   
 ρ air density  
 h turbine blade height  
 λ tip speed ratio  $\lambda = (nR)/U_{\infty}$   
 R turbine radius  
 CP turbine power coefficient  $C_P = C_m \times \lambda$   
 Cm turbine moment coefficient  
 VAWT vertical axis wind turbine  
 SKE standard k-ε  
 SSTKW shear stress transport k-ω

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