



Review on Sensitivity Analysis of a Dual-Mechanical-Port Bi-Directional Machine

Harish Harsurkar¹, Dr.G.R.Selokar², Dr.B Nageshwar Rao³

Research Scholar, SSSUTMS, Sehore (M.P), India¹

Professor, SSSUTMS, Sehore, Bhopal, M.P, India²

Professor, Mahaveer Institute of Science & Technology, Hyderabad³

ABSTRACT

This examination presents an ideal plan technique of a double mechanical-port bidirectional flux modulated machine for electric consistently factor transmission in HEV. The machine uses bidirectional motion regulation impact to consolidate one stator and two rotors, meaning to acknowledge electrical and mechanical force adaptable split and mix. Because of the intricacy of the machine structure, traditional improvement techniques utilizing investigative model are unimportant. Consequently, a successful and viable strategy which consolidates the hereditary calculation and limited component technique is proposed to improve the plan of the machine. When the computational cost increments exponentially with the expanding of number of plan boundaries, to decrease the computational expense in the streamlining cycle, the plan boundaries are partitioned as 2 levels basing on an affectability examination. And afterward the delicate boundaries are upgraded utilizing the GA-FEM coupled strategy.

Key words : Sensitivity, Bi-directional, Machine, hybrid electric vehicles, DR-FBMM, GA-FEM.

1. INTRODUCTION

Because of the rising worries of the ecological issues and energy emergency, elective energy vehicles have been a mainstream field for specialists. With phenomenal energy proficiency and exceptional driving execution, half and half electric vehicles (HEVs) have gotten incredible business accomplishment in the most recent decade. For the most part, the HEVs are grouped into three kinds which are the arrangement crossover vehicles, the equal half and half vehicles and the arrangement equal mixture geography. The arrangement equal half and half geography can kill the disadvantages of arrangement mixture and equal cross breed geography and gives improved energy transformation

execution. As the most celebrated HEV, Toyota Prius embraces the arrangement equal geography and utilize a planetary apparatus framework to understand the force parting and blend. The planetary rigging framework is likewise named as consistently factor transmission (CVT) framework. It is a significant and essential segment in cutting edge arrangement equal half breed EVs, which goes about as a force parting unit to guarantee the ideal activity of the inner ignition motor (ICE) paying little mind to the speed varieties of the vehicle. In any case, the planetary apparatus likewise brings a few deformities, for example, low mechanical unwavering quality, perceptible commotion and high support cost. Restricted by the inadmissible execution of battery advancements and the significant expense of power devices, HEVs are the most ideal decision to connect the flow circumstances and the requests for energy-efficient transportation. As per the kinds of the force train, HEVs can be commonly named arrangement HEVs, equal HEVs and force split HEVs, in which the powersplit HEVs join the advantages of both the equal sorts and the arrangement types, consequently offering the benefits of super low outflows and high mileage [1]. The electronic-constantly factor transmission (E-CVT) framework is one of the center parts for the force split HEVs [2]. It was right off the bat received by Toyota Prius in 1997 [3]. At that point, a few subordinates compound split ECVT were presented.

2. LITERATURE REVIEW

Chau et al proposed with ever-expanding worries on our condition, there is a quickly developing enthusiasm for EVs and it is a squeezing requirement for specialists to create progressed electric-drive systems[1].

Xu et al proposed a serious full half and half electrical vehicle, the little IC motor runs just in a limited speed go for the most elevated energy effectiveness[3].

Shuangxia et al proposed novel twofold stator, twofold rotor brushless electrical constantly factor transmission framework is proposed[4].

Xiang et al proposed a brushless twofold mechanical port transition exchanging lasting magnet engine for expected application in half and half electric vehicles. To understand the plan goals of high-force ability, low-force wave, and low-attractive coupling between the internal and external engines, another staggered plan streamlining strategy is proposed to direct a multiobjectives optimization[5].

3. METHODOLOGY

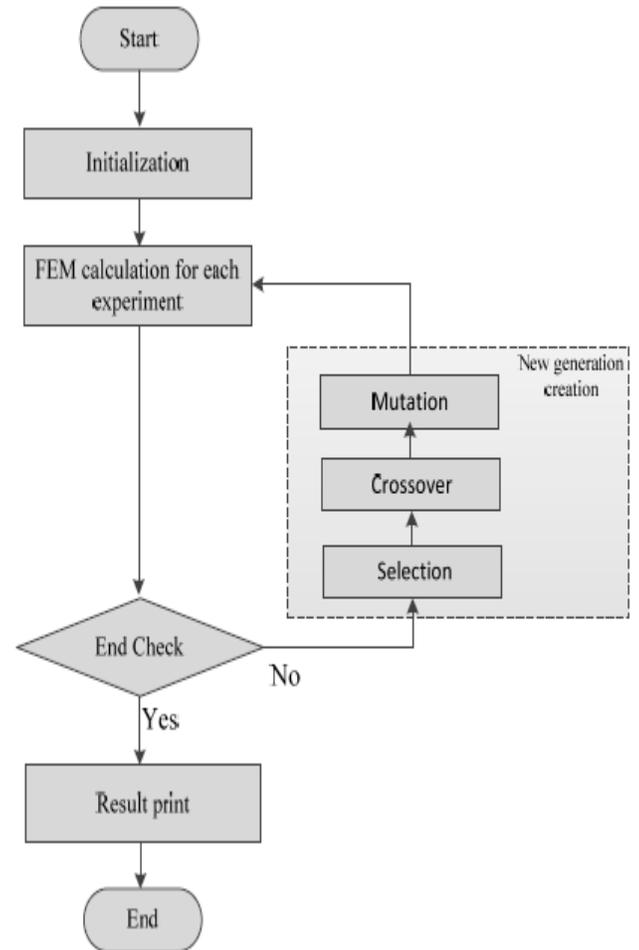
The framework offers an electric answer for constantly factor transmission of the mixture EVs. This electric consistently factor transmission framework coordinates the benefits of the double rotor machine and the motion regulation machine and appreciates extra advantages, for example, high force thickness and minimal effort halfway scale converter. The activity guideline, motion balance rule and consistent execution of the machine are researched. Time venturing limited component technique is utilized to dissect the dynamic presentation of the proposed framework. Novel double rotor machine with transition regulation structure is proposed and named as double rotor motion bidirectional adjustment machine. The motion adjustment machine is likewise magnet gear machine. In the two structures, the transition regulation impact is utilized to enhance the force thickness. In this way, the FMM is truly reasonable for the high force thickness, legitimately driving framework. Contrasted and the ordinary DRM, the novel transition balance machine effectively disposes of the brushes. In this external rotor PM shafts of the attractive rigging are supplanted by the stator windings and lasting magnets and balance prepares are then again organized on the center and internal rotors. The rotor back EMF is shown in below equation.

$$f_p = N_l \omega_1 - N_s \omega_2$$

To lessen the calculation cost and improvement, the boundaries are separated into 2 dependent on the affectability examination, specifically the delicate boundaries and non-touchy boundaries. The affectability uncovers the connection transport between the boundary and the target. Notwithstanding the communication impacts among the boundaries, the affectability of a boundary shows its impact on estimation of the goal work. The choice of the underlying plan of the DF-BFM is significant for the exactness of the affectability examination.

4. OPERATION MODES OF PMDMP MACHINE

The PMDMP machine has very high control flexibility because its dual-mechanical port and dual-electrical-port



structure provides many operational possibilities. If the power losses are neglected, the relationship between the mechanical and electrical power can be represented by (1).

Fig.1 The GA-FEM methodology

$$P_{es} + P_{eir} + P_{mICE} - P_{mWheel} = 0 \tag{1}$$

P_{es} is the electrical power provided by the stator windings; P_{eir} is the electrical power. Theoretical speaking, all the powers in (1) can be bidirectional. However, some of the scenarios are not likely to occur during steady state operation. For example, the mechanical power from the ICE (P_{mICE}) is not likely to be negative, because the ICE cannot consume mechanical power.

$$P_{es} = (T_{eor} + T_{eir})\omega_{or}, P_{eir} = -T_{eir}(\omega_{or} - \omega_{ir}), P_{mICE} = T_{ICE}\omega_{ir} = -T_{eir}\omega_{ir} \text{ and } P_{mWheel} = T_{eor}\omega_{or}. \quad (2)$$

$$(T_{eor} + T_{eir})\omega_{or} - T_{eir}(\omega_{or} - \omega_{ir}) - T_{eir}\omega_{ir} - T_{eor}\omega_{or} = 0 \quad (3)$$

The total electrical input power from both the windings equals to the power provided by the battery, thus the battery output power can be expressed by (4)

$$P_{battery} = P_{es} + P_{eir} = (T_{eor} + T_{eir})\omega_{or} - T_{eir}(\omega_{or} - \omega_{ir}) = T_{eor}\omega_{or} + T_{eir}\omega_{ir} = P_{mWheel} - P_{mICE} \quad (4)$$

Three important observations can be obtained from (4). First, the two energy sources of the system, i.e., the battery and the ICE, work together to drive the vehicle ($P_{battery} + P_{mICE} = P_{mWheel}$). Second, the inner rotor windings provides positive electrical power to the system and this part of power is called the slip power (if $\omega_{or} > \omega_{ir}$, then $P_{eir} = -(\omega_{or} - \omega_{ir}) = T_{ICE}(\omega_{or} - \omega_{ir}) > 0$). Third, the mechanical power from the ICE is transferred to the wheels directly without flowing into the battery.

To better explain the power flow of the PMDMP machine, the constant power mode is selected as an example. The constant power mode means the mechanical input power from the ICE equals to the mechanical output power of the vehicle ($P_{mICE} = P_{mWheel}$). Note that power losses are neglected for simplicity of discussion. Thus (5) is satisfied.

$$P_{battery} = P_{es} + P_{eir} = P_{mICE} - P_{mWheel} = 0 \quad (5)$$

5. CONCLUSION

In this paper we have discussed about sensitivity analysis of bi-directional machine. To diminish the calculation cost of the GA-FEM streamlining, the boundaries are isolated into 2 classes dependent on the affectability investigation. The choice of the underlying plan of the DF-BFM is significant for the precision of the affectability examination.

REFERENCES

[1] K. T. Chau, C. C. Chan, and C. Liu, “**Overview of permanent-magnet brushless drives for electric and hybrid electric vehicles,**” IEEE Trans. Ind. Electron., vol. 55, no. 6, pp. 2246–2257, Jun. 2008.

[2] J. Druant, H. Vansompel, F. D. Belie, J. Melkebeek and P. Sergeant. “**Torque analysis on a double rotor electrical variable transmission with hybrid**

excitation,” IEEE Trans. Ind. Electron., vol. 64, no. 1, pp. 60–68, Jan. 2017.

[3] L. Xu, Y. Zhang, and X. Wen, “**Multioperational modes and control strategies of dual-mechanical-port machine for hybrid electrical vehicles,**” IEEE Trans. Ind. Appl., vol. 45, no. 2, pp. 747–755, Mar./Apr. 2009.

[4] S. Niu, S. L. Ho and W. N. Fu, “**A novel double-stator double-rotor brushless electrical continuously variable transmission system,**” IEEE Trans. Magn., vol. 49, no. 7, pp. 3909–3912, July. 2013.

[5] Z. Xiang, X. Zu, L. Quan, Y. Du, C. Zhang and D. Fan, “**Multilevel design optimization and operation of a brushless double mechanical port flux-switching permanent-magnet motor,**” IEEE Trans. Ind. Electron., vol. 63, no. 10, pp. 6042–6054, Oct. 2017.

[6] K. Atallah, S. D. Calverley, and D. Howe, “**Design, analysis and realisation of a high-performance magnetic gear,**” Inst. Electr. Eng. Proc. Electr. Power Appl., vol. 151, no. 2, pp. 135–143, Mar. 2004.

[7] S. L. Ho, S. Niu, and W. N. Fu, “**Design and Comparison of Vernier Permanent Magnet Machines,**” IEEE Trans. Magn., Vol. 47, No. 10, pp. 3280–3283, Oct. 2011.

[8] K. T. Chau, D. Zhang, J. Z. Jiang, C. Liu and Y. Zhang, “**Design of a magnetic-g geared outer-rotor permanent-magnet brushless machine for electric vehicles,**” IEEE Trans. Magn., vol. 43, no. 6, pp. 2504–2506, Jun. 2007.

[9] Y. Oner, Z. Q. Zhu, L. J. Wu, X. Ge, Hanlin Zhan and J. T. Chen, “**Analytical on-load subdomain field model of permanent-magnet Vernier machines,**” IEEE Trans. Ind. Electron., vol. 63, no. 7, pp. 4105–4117, Feb. 2016.

[10] Y. Fan, L. Zhang, M. Cheng and K. T. Chau, “**Sensorless SVPWMFADTC of a new flux-modulation permanent-magnet wheel motor based on a wide-speed sliding mode observer,**” IEEE Trans. Ind. Electron., vol. 62, no. 5, pp. 3143–3151, Dec. 2014.

[11] S. L. Ho, S. Niu and W. N. Fu, “**Design and analysis of a novel axialflux electric machine,**” IEEE Trans. Magn., vol. 47, no. 10, pp. 4368–4371, Sep. 2011.

[12] L. Xu, G. Liu, W. Zhao, X. Yang and R. Cheng, “**Hybrid stator design of fault-tolerant permanent-magnet Vernier machines for direct-drive applications,**” IEEE Trans. Ind. Electron., vol. 64, no. 1, pp. 179–190, Jan. 2017

[13] D. Li, R. Qu, and T. Lipo, “**High power factor vernier permanent magnet machines,**” IEEE Trans. Ind. Appl., vol. 50, no. 6, pp. 3664–3674, Nov./Dec. 2014.

- [14] W. Zhao, J. Zheng, J. Wang, G. Liu, J. Zhao, Z. Fang, **“Design and Analysis of a Linear Permanent-Magnet Vernier Machine With Improved Force Density,”** IEEE Trans. Ind. Electron., vol. 63, pp. 2072- 2082, Apr. 2016.
- [15] L. Sun, M. Cheng, and H. Jia, **“Analysis of a novel magnetic-g geared dual rotor motor with complementary structure,”** IEEE Trans. Ind. Electron., vol. 62, no. 11, pp. 6737–6747, Nov. 2015.
- [16] J. Bai, P. Zheng, C. Tong, Z. Song and Q. Zhao, **“Characteristic analysis and verification of the magnetic-field modulated brushless double-rotor machine”**, IEEE Trans. Ind. Electron., vol. 62, no. 7, pp. 4023–4033, Jul. 2015.
- [17] S. Niu, S. L. Ho, and W. N. Fu, **“Design of a novel electrical continuously variable transmission system based on harmonic spectra analysis of magnetic field,”** IEEE Trans. Magn., vol. 49, no. 5, pp. 2161–2164, May 2013.