Vector controlled PMSM Drive based on Fuzzy Speed Controller

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ABSTRACT

To improve the dynamic performances of Permanent Magnet Synchronous Motor (PMSM) drive, a novel implementation of speed controller based on adaptive fuzzy logic is presented in this paper. Using the output of the Fuzzy speed Controller (FC), the quadrature axis current reference value can be obtained. At the same time, the outputs of the current controller can be corrected by the disturbance voltage observer's outputs. Results of simulation are provided to demonstrate the effectiveness of the proposed scheme under the occurrence of parameter variations and external disturbance.

Keywords: PMSM; Fuzzy Controller; disturbance voltage observer; PI Controller; Vector Control Technique.

I. INTRODUCTION

For vector controlled PMSM drives, the conventional speed controller such as proportional integral (PI) controller can't give satisfactory performance when the running conditions changed [1,2].

Nowadays, some adaptive controllers have been applied in both ac and dc motor drive. Such as model reference adaptive controller (MRAC) [3] and sliding model controller (SMC) [4], etc. all the types of controllers can improve the performance of the motor drive system. However, they are usually based on the parameters and structure of the system model. It will lead to complex computation when the system model is uncertainty .

Fuzzy controllers have been applied to many industrial fields, and it does not need mathematical model of the controlled system. In [5], the fuzzy controller instead of the traditional hysteresis controller is proposed in direct torque controlled PMSM drives, the appropriate voltage vector can be selected according to torque and flux settings the ability to deal with uncertain information of the fuzzy logic. In [6], a scheme of establishing fuzzy speed controller is introduced. They all achieve satisfactory results to some extent.

In this paper, the conventional PI speed controller is replaced by the fuzzy controller, when the parameters of PMSM is changed, voltage compensation term can be obtained by a disturbance voltage observer. Vector controlled PMSM drive provides better dynamic response and lesser torque ripples, and necessitates only a constant switching frequency.The proposed control scheme has been testified by simulation, the results indicate the PMSM drive with the adaptive fuzzy controller will have the ability of quick recovery of the speed from any disturbances and parameters variation. Accordingly, the proposed PMSM drive will have better dynamic performances and robustness.

2. DISTURBANCE VOLTAGE OBSERVER OF THE PMSM

The vector control technique was firstly proposed for induction motors, while it was applied to PMSM later. Its basic principle is to decouple the stator current to get direct axis (d-axis) and quadrature axis (q-axis) components. The vector control strategy is formulated in the synchronously rotating reference frame. An efficient control strategy of the vector control technique is to make the d-axis current id zero so that the torque becomes dependent only on q-axis current.

The stator voltage equations of a PM synchronous motor in the synchronously rotating reference frame are described as follows

$$u_d = R_s i_d + L_d i_d - L_q \omega_r i_q \qquad (1)$$
$$u_q = R_s i_q + L_q i_q + L_d \omega_r i_d + \psi_f \omega_r$$

Where

u_d d-axis voltage in synchronous frame,[V];
u_q q-axis voltage in synchronous frame, [V];
Rs   motor phase resistance, [Ω];
L_d d-axis inductance, [H];
L_q q-axis inductance, [H];
i_d d-axis current in synchronous frame, [A];
i_q q-axis current in synchronous frame, [A];
ω_r motor electrical angular velocity, [Rad/s];
ψ_d d-axis flux linkage in synchronous frame,[Wb];
ψ_q q-axis flux linkage in synchronous frame, [Wb];
ψ_f PM flux linkage in synchronous frame, [Wb].

Accordingly, the discrete-time equation can be obtained as follows[7,8]

$$u_d(n) = R_s i_d(n) + \frac{L_d}{T}[i_d(n) - i_d(n-1)] - L_q \omega_r i_q(n) \qquad (2)$$

$$u_q(n) = R_s i_q(n) + \frac{L_q}{T}[i_q(n) - i_q(n-1)] + L_d \omega_r i_d(n) + \psi_f \omega_r \qquad (3)$$

where T is the sampling period.

When the parameters of PMSM vary during the operation, it will cause the disturbances f_d (n) and f_q (n), giving[7]

$$f_d(n) = \Delta\, R_s i_d(n) + \frac{\Delta L_d}{T}[i_d(n) - i_d(n\text{-}1)] - \Delta\, L_q \omega_r i_q(n) \qquad \textbf{(4)}$$

$$f_q(n) = \Delta\, R_s i_q(n) + \frac{\Delta L_q}{T}[\, i_q(n) - i_q(n\text{-}1)] + \Delta L_d \omega_r i_d(n) + \Delta\, \psi_f\, \omega_r \quad \textbf{(5)}$$

where $\Delta\, R_s = R_s - R_{s0}$, $\Delta L_d = L_d - L_{d0}$, $\Delta L_q = L_q - L_{q0}$, $\Delta\, \psi_f = \psi_f - \psi_{f0}$ and subscript "0" denotes the nominal value.

The steady-state response of the predictive control can be effectively improved by using a simple time delay control approach. In the time delay control, it is considered that the values of $f_d(t)$, $f_q(t)$ and at the present time are very close to those at time t-τ (τ = LT) in the past for a small time τ delay, and can be expressed
when L=I is chosen as follows[8]

$$f_d(n) \approx f_d(n\text{-}1) \qquad \textbf{(6)}$$
$$f_q(n) \approx f_q(n\text{-}1)$$

By approximating the disturbances at the present time with those of (n-1)th time step and using (5) and (6), the simple estimates for the disturbances can be derived as follows[7]

$$\hat{f}_d(n) \approx u_d(n) - [R_{S0}\, i_d(n) + \frac{\Delta L_{d0}}{T}[i_d(n) - i_d(n\text{-}1)] - \Delta L_{q0}\omega_r i_q(n) \quad \textbf{(7)}$$

$$\hat{f}_q(n) \approx u_q(n) - [R_{S0}\, i_q(n) + \frac{\Delta L_{q0}}{T}[\, i_q(n) - i_q(n\text{-}1)] + \Delta L_{d0}\omega_r i_d(n)$$
$$+ \Delta\, \psi_{f0}\, \omega_r \qquad \textbf{(8)}$$

Taking into account equation (7) and (8) contain high-order harmonic components, in the application process, a low-pass filter is needed. Therefore, disturbances voltage caused by the parameters changes can be expressed as[7]

$$\hat{f}_{df}(n) = \frac{2 - aT}{2 + aT}\, \hat{f}_{df}(n\text{-}1) + \frac{aT}{2 + aT}\, [\hat{f}_d(n) + \hat{f}_d(n\text{-}1)] \qquad \textbf{(9)}$$

$$\hat{f}_{qf}(n) = \frac{2 - aT}{2 + aT}\, \hat{f}_{qf}(n\text{-}1) + \frac{aT}{2 + aT}\, [\hat{f}_q(n) + \hat{f}_q(n\text{-}1)] \qquad \textbf{(10)}$$

Under the occurrence of parameter variations and external disturbance, the disturbances voltage, by which u_d^* u_q^* and will be revised on-line, can be calculated from equation (9) and (10).

3.STRUCTURE OF FUZZY SPEED CONTROLLER

Most of the PMSM controllers for industrial applications adopt a fixed-gain PI scheme. This fixed-gain scheme may work fine under certain operating conditions, but degrades its performance under other operating conditions. Moreover, suitable PI gains are usually obtained using time-consuming trial-and-error methods. To increase the performances of PMSM drive, an adaptive speed controller based on fuzzy logic is proposed. The block diagram of the proposed scheme is illustrated in Fig.I.

The output of the fuzzy speed controller is the reference value of quadrature axis current i_q^* the inputs are esl, es2, and can be expressed as follows, respectively.

$$e_{s1}(n) = \omega_r^*(n) - \omega_r(n)$$

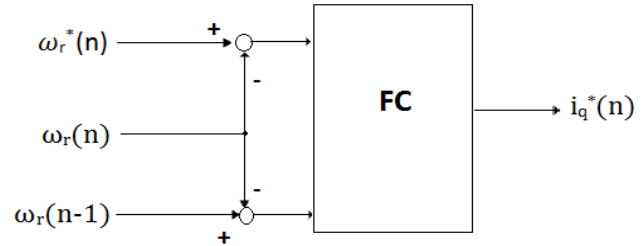$$e_{s2}(n) = \omega_r(n-1) - \omega_r(n)$$

Figure (1):.Membership Functions of FC

The inputs are the estimate value of the disturbance voltage observer $\hat{f}_{df}(n)$ and $\hat{f}_{qf}(n)$.

The universe of all input and output variables are normalized to [-1 1]. The fuzzy membership functions of the input variables and output variable of the fuzzy controller are shown in Fig 2. And the corresponding fuzzy logic rule is shown in Tabel 1. respectively.

In real time implementation, using the reference speed and the actual speed, we can calculate e_{sl} and e_{s2}, and the new reference value of the quadrature axis current i_q^* can be obtained from the speed fuzzy controller. Once the parameter variations and external disturbance appear, the reference values of quadrature axis and direct axis voltage will be revised by the output of the disturbance voltage observer.

Table 1.The Fuzzy Logic Rule

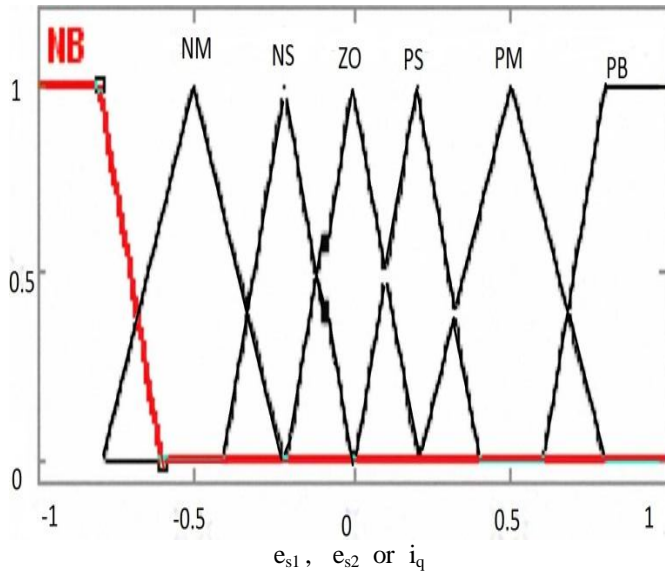| e_{s1} \ e_{s2}	NB	NM	NS	ZO	PS	PM	PB
NB	NB	NB	NM	NM	NS	ZO	ZO
NM	NB	NB	NM	NS	NS	ZO	PS
NS	NM	NM	NM	NS	ZO	PS	PS
ZO	NM	NM	NS	ZO	PS	PM	PM
PS	NS	NS	ZO	PS	PS	PM	PM

Figure (2): Membership Functions

4. RESULTS OF SIMULATION

A block diagram of the proposed PMSM drive is shown in Fig 3. The parameters of PMSM are shown in Table 2. And the availability is conformed by computer simulations. The simulation conditions are: $J= I.5J_o$, $R_S = 2R_{S0}$, $\psi_f = 0.8 \; \psi_{f0}$, $L_d = 1.3L_{d0}$, $L_q =1.3L_{q0}$, and $n^* =1800r/min$, $T_z =100N.m.$, The results

under the PI speed controller and the proposed scheme are shown in Fig A and Fig.5, respectively.

Under the above-mentioned simulation conditions, Fig. 4 and Fig. 5 show that the dynamic response performances of the PMSM drive based on the proposed scheme has been improved to some extent compared with the system based on the conventional PI speed controller.

Table 2. Parameters of PMSM

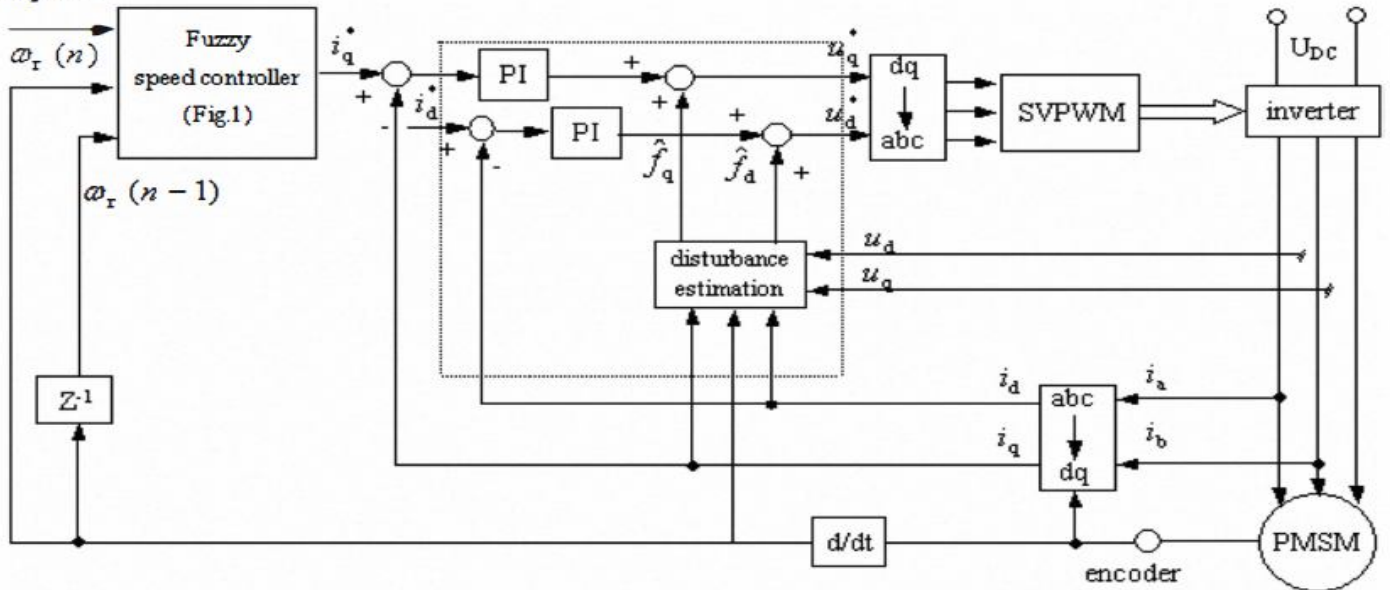| Rated voltage $U_N(V)$	440
Rated speed (r/min)	1800
Rated current (A)	90
Stator resistance R_S (Ω)	0.06
d-axis stator inductance L_d (mH)	2.562
q-axis stator inductance L_q (mH)	3.080
Rotor flux linkage ψ_f (Wb)	0.69

Figure (3): Overall block diagram of PMSM drive based on the proposed control scheme
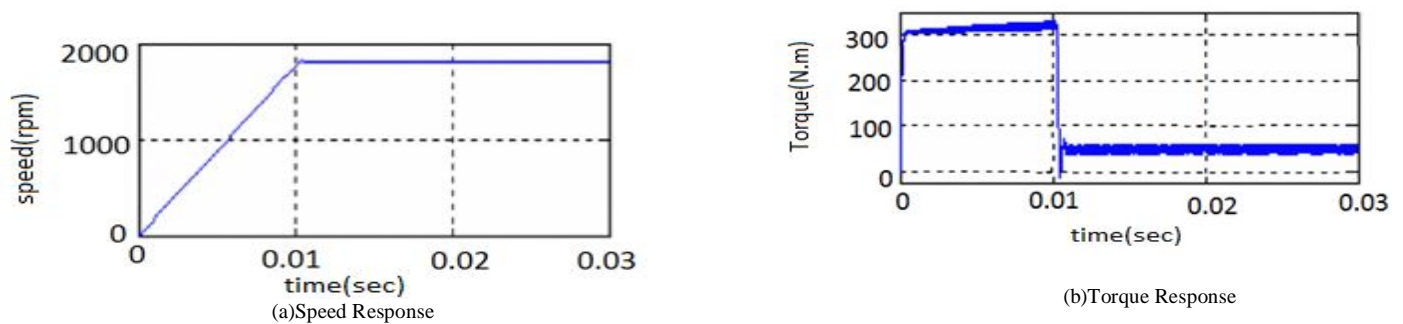
(a)Speed Response

(b)Torque Response

Figure (iii): Resluts of PMSM control drive based on PI speed

(a)Speed Response
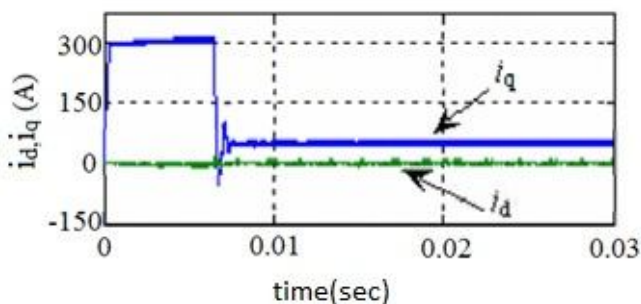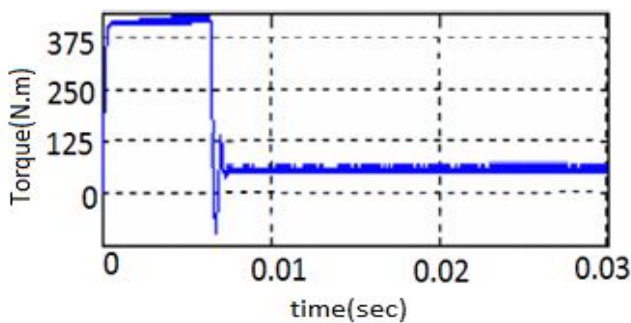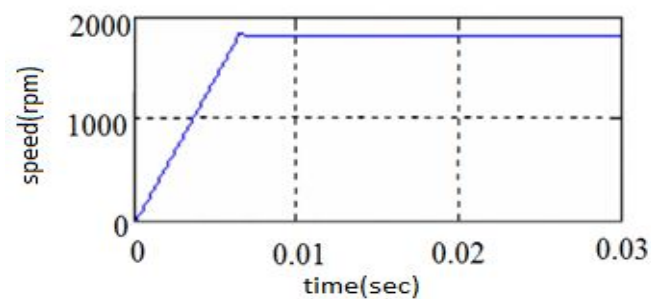

(b)Torque Response

(c)Current Response

Figure (5): Resluts of PMSM control drive based on Proposed scheme

5. CONCLUSION

In this paper, a vector control scheme with the fuzzy speed controller with the disturbance voltage observer for the PMSM has been presented. It combines the capability of fuzzy reasoning in handling uncertain information and the ability to compensate of the disturbance voltage observer on-line. The results of simulation have shown that the PMSM drive with the proposed control scheme has the merits of simple structure, robustness, quick tracking performance.

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